

MAGNETO STATICS - I

Biot-Savart's Law and its applications : Static magnetic fields - Biot-Savart's Law - Magnetic field intensity (MFI) - MFI due to a straight current carrying filament - MFI due to Circular, Square and Solenoid current carrying wire - Relation between magnetic flux, magnetic flux density and MFI - Maxwell's equation

Ampere's circuital law and its applications : MFI due to an infinite sheet of current and a long current carrying filament - point form of Ampere's circuital law - Maxwell's equation. Field due to a circular loop, rectangular and square loops.

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Introduction:

- Uptill now static electric fields are discussed. The electrostatic field exists due to the static charges i.e., charges are at rest.
- The magnetic field exists due to permanent magnet, which is a natural magnet.  
But there is ~~no~~ link absent b/w electric field and magnetic field due to natural magnet.
- A definite link between electric and magnetic fields was established by Oersted in 1820. As we have noticed, an electrostatic field is produced by static or stationary charges. If the charges are moving with constant velocity, a static magnetic (or magnetostatic) field is produced.
- A magnetostatic field is produced by a constant current flow (or direct current).

- Magnetostatics deals with magnetic field produced by current carrying conductor.
- The study of steady magnetic field, existing in a given space produced due to the flow of direct current through a conductor is called "Magnetostatics".
- A static magnetic field can be produced from a permanent magnet or a current carrying conductor.

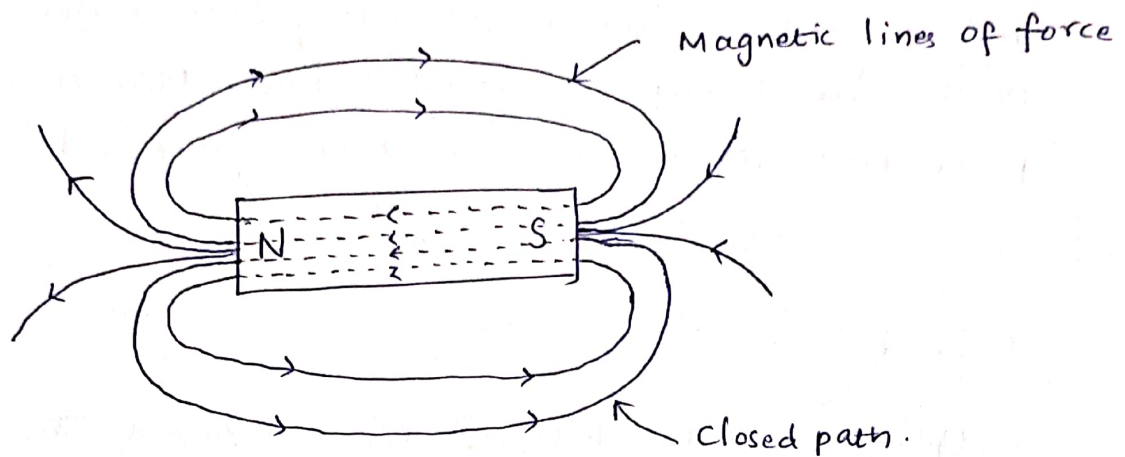


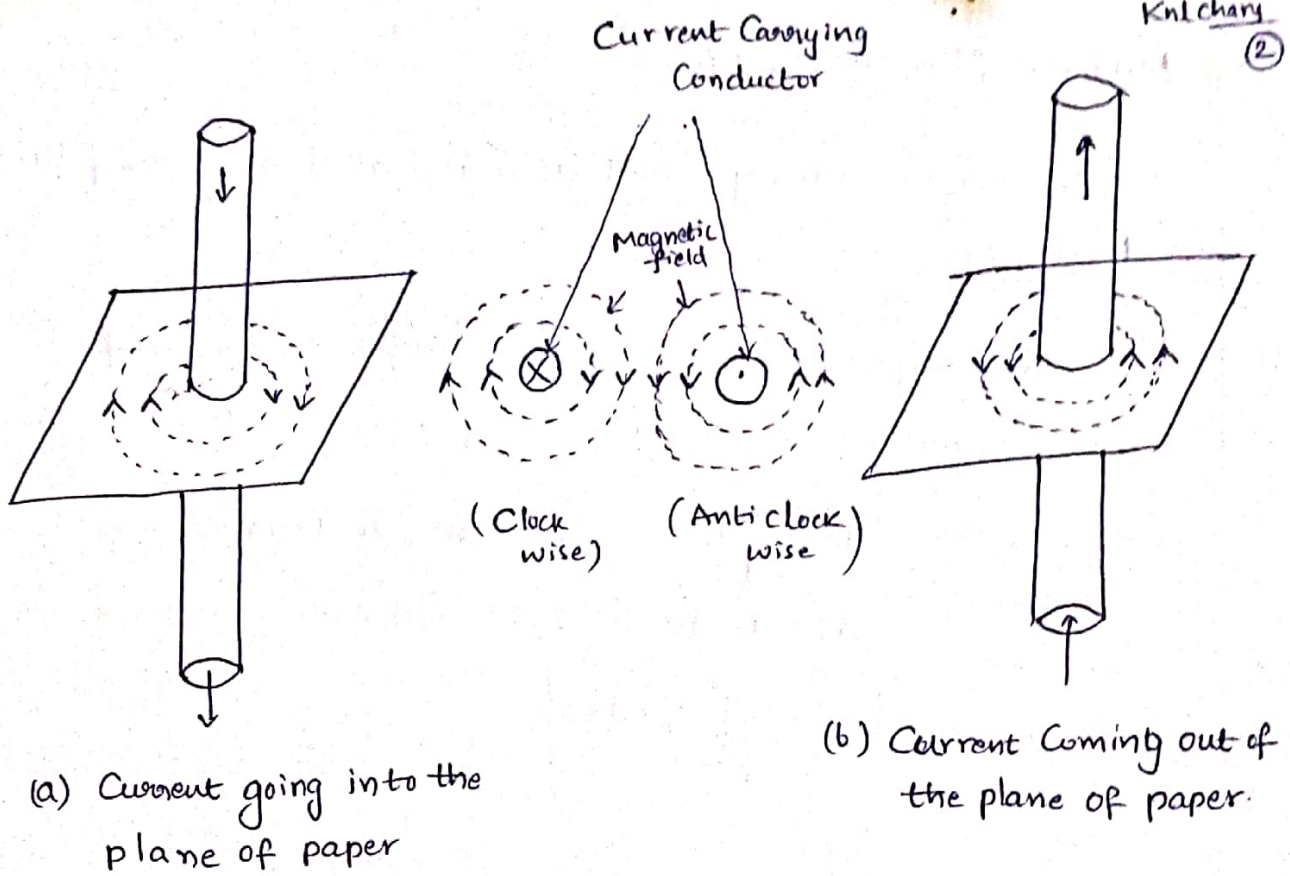
Fig: permanent magnet and magnetic lines of force.

**[NOTE]** An isolated magnetic pole can not exist.

- The magnetic lines of force are also called magnetic lines of flux or magnetic flux lines.
- Hence every magnetic flux line starting from North pole must end at South pole and complete the path from South to North internal to the magnet.

**[NOTE]** The magnetic flux lines exist in the form of closed loop.

- Magnetic field: The region around a magnet within which the influence of the magnet can be experienced is called magnetic field.



→ When a straight Conductor Carries a direct current, it produces a magnetic field around it in the form of Concentric circles.

→ ⊗ - Cross indicates that the current direction is going into the plane of the paper away from the observer.

⊙ - dot indicates that the current direction is coming out of the plane of the paper coming towards the observer.

→ Right Hand Thumb Rule is used to determine the direction of field around a current carrying conductor.

Thumb → pointing the direction of ~~the~~ Current.

Curled fingers → pointing the direction of magnetic lines of flux around the conductor.

## Magnetic flux density ( $\vec{B}$ ):

The magnetic flux per unit area is called magnetic flux density ( $\vec{B}$ ).

→ The magnetic flux through any surface is the surface integral of the normal component of  $\vec{B}$ .

$$B = \frac{d\phi}{da} \quad \text{Wb/m}^2 \text{ or Tesla.}$$

$$d\phi = B \cdot da.$$

$$\phi = \iint_S \vec{B} \cdot d\vec{a}$$

## Magnetomotive force (M.M.F):

M.M.F is produced when an electric current flows through a coil of several turns. The M.M.F depends on the current and the number of turns.

$$\text{M.M.F} = NI \quad \text{Ampere Turns.}$$

## Magnetic field Intensity ( $\vec{H}$ ) (or)

### Magnetic field strength

Magnetic field intensity at any point in the magnetic field is defined as the force experienced by the unit north pole of one weber strength, when placed at that point.

(or)

MFI is defined as the ratio of M.M.F to meter length.

$$\vec{H} = \frac{\text{M.M.F}}{\text{length}} = \frac{NI}{l}$$

$$\text{N/Wb or AT/m or A/m}$$

Units: Newton/weber or Ampere Turns/meter or Ampere/meter.

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Reluctance: Reluctance is the opposition to the establishment of magnetic flux and can be defined as the ratio of M.M.F to the flux produced.

$$\text{Reluctance, } R = \frac{\text{M.M.F}}{\text{magnetic flux}} = \frac{NI}{\Phi} \quad \text{AT/Wb}$$

- There are two major laws governing magnetostatic fields:  
(1) Biot-savart's law and (2) Ampere's Circuit law.
- Like Coulomb's law, Biot-Savart's law is the general law of magnetostatics.
- Just as Gauss's law is a special case of Coulomb's law, Ampere's law is a special case of Biot-Savart's law and easily applied in problems involving symmetrical current distribution.

## BIOT - SAVART'S LAW

→ Biot - Savart's law states that the differential magnetic field intensity  $d\vec{H}$  produced at a point P, by the differential current element  $I d\vec{l}$  is

- (i) proportional to the product  $I d\vec{l}$  and the sine of the angle  $\alpha$  between the element and the line joining P to the element and (ii) inversely proportional to the square of the distance  $R$  between P and the element.

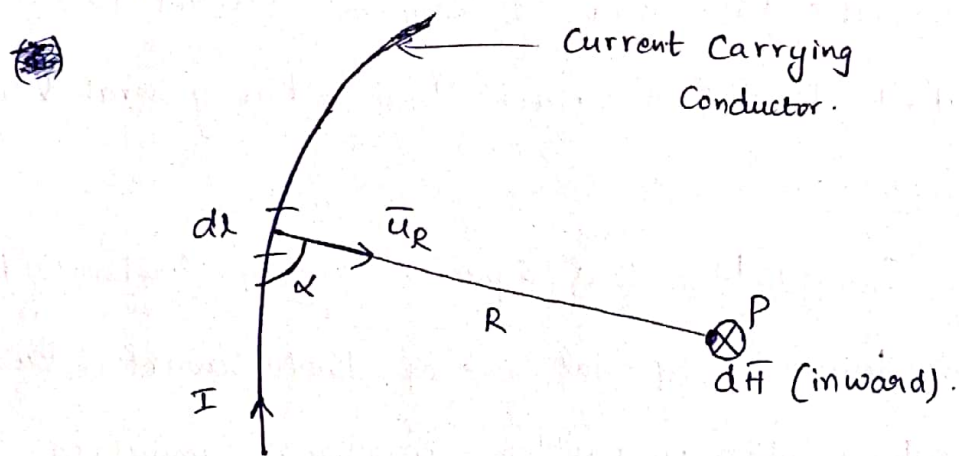


Fig: Magnetic field  $d\vec{H}$  at P due to Current element  $I d\vec{l}$ .

$dl \rightarrow$  Differential length

$I d\vec{l} \rightarrow$  Differential Current element

$d\vec{H} \rightarrow$  Differential magnetic field intensity

$R \rightarrow$  Distance between P and the element.

$\alpha \rightarrow$  Angle b/w the element and the line joining P to the element.

$\vec{u}_r \rightarrow$  Unit vector directed from element to P.

Mathematical Representation

$$d\vec{H} \propto \frac{I dl \sin \alpha}{R^2}$$

$$d\vec{H} = \frac{K I dl \sin \alpha}{R^2}$$

where  $K = \text{Constant of proportionality}$   
 $= \frac{1}{4\pi}$

$$d\vec{H} = \frac{I dl \sin \alpha}{4\pi R^2}$$

$$d\vec{H} = \frac{I dl \times \vec{u}_R}{4\pi R^2}$$

$$d\vec{H} = \frac{I dl \times \vec{R}}{4\pi R^3} \quad \left[ \because \vec{u}_R = \frac{\vec{R}}{|\vec{R}|} \right]$$

$$\Rightarrow \boxed{d\vec{H} = \frac{I dl \times \vec{u}_R}{4\pi R^2} = \frac{I dl \times \vec{R}}{4\pi R^3}} \quad \text{A/m}$$

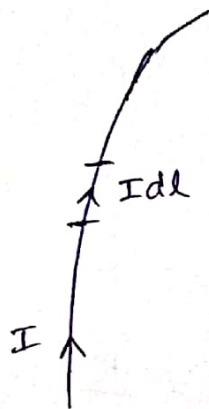
→ The direction of  $d\vec{H}$  can be determined by the right-hand rule with the right-hand thumb pointing the direction of the current and right-hand curled fingers encircling the wire in the direction of  $d\vec{H}$ .

→ It is customary to represent the direction of magnetic field intensity  $\vec{H}$  (or current  $I$ ) by a small circle with a dot or cross sign depending on whether  $\vec{H}$  or ( $I$ ) is out of page, or into it respectively.

$$\vec{H} = \oint \frac{I d\vec{l} \times \vec{u}_R}{4\pi R^2} = \oint \frac{I d\vec{l} \times \vec{R}}{4\pi R^3}$$

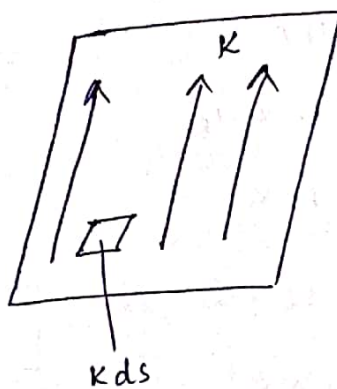
$$\vec{B} = \oint \frac{\mu I d\vec{l} \times \vec{u}_R}{4\pi R^2} = \oint \frac{\mu I d\vec{l} \times \vec{R}}{4\pi R^3}$$

Different Current distributions:



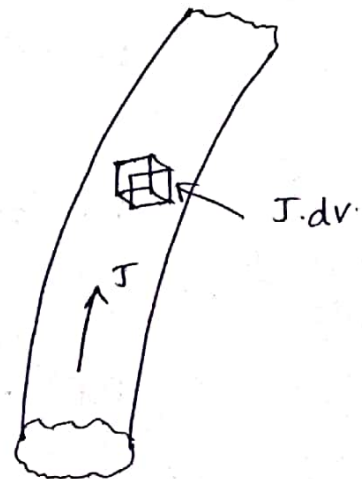
(a)

$K$  = Surface Current density (A/m)



(b)

$J$  = Volume Current density (A/m<sup>2</sup>)



(c)

The Source elements are related as

$$I d\vec{l} \equiv K \cdot d\vec{s} \equiv J \cdot d\vec{v}$$

Thus in terms of distributed Current Sources, the Biot-Savart's law

$$H = \int_L \frac{I d\vec{l} \times \vec{u}_R}{4\pi R^2} \quad (\text{Line Current})$$

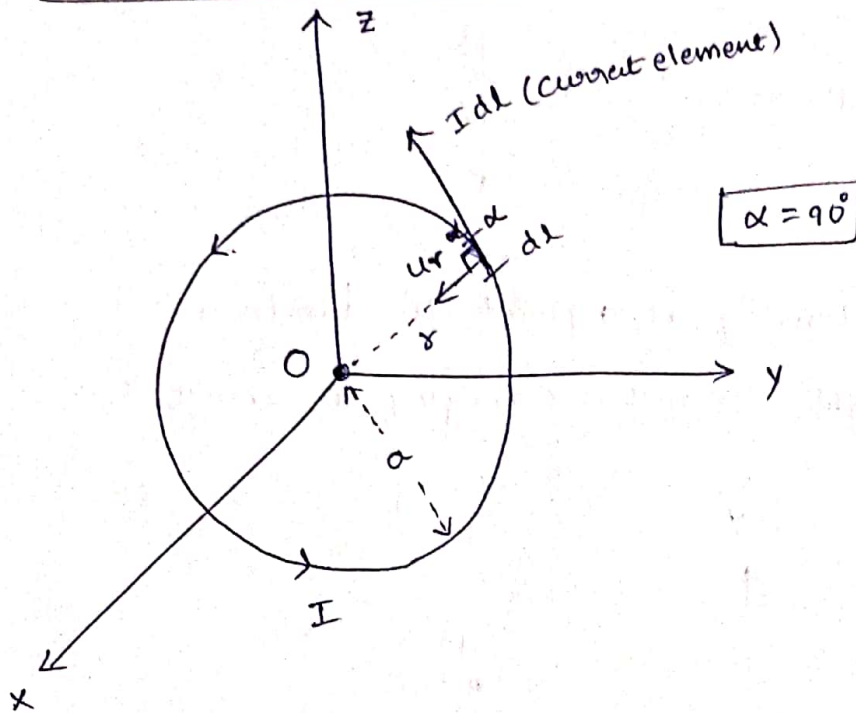
$$H = \int_s \frac{K d\vec{s} \times \vec{u}_R}{4\pi R^2} \quad (\text{Surface Current})$$

$$H = \int_v \frac{J d\vec{v} \times \vec{u}_R}{4\pi R^2} \quad (\text{Volume Current}).$$

where  $\vec{u}_R$  is a unit vector pointing from differential element of Current to the point of interest.

## Examples:

- (1) Field Intensity  $\vec{H}$  at the Centre of Circular wire Carrying Current,  $I$  :



→ The field intensity at O is given by  $\vec{H} = \oint d\vec{H}$

where  $d\vec{H}$  is the field intensity at O due to any current element  $I dl$ .

According to Biot-Savart's Law

$$d\vec{H} = \frac{I dl \sin 90^\circ}{4\pi a^2} \hat{k} \quad \left[ \because \alpha = 90^\circ \right. \\ \left. r = a \right]$$

$$d\vec{H} = \frac{I dl}{4\pi a^2} \hat{k}$$

$$\vec{H} = \oint d\vec{H} = \oint \frac{I dl}{4\pi a^2} \hat{k}$$

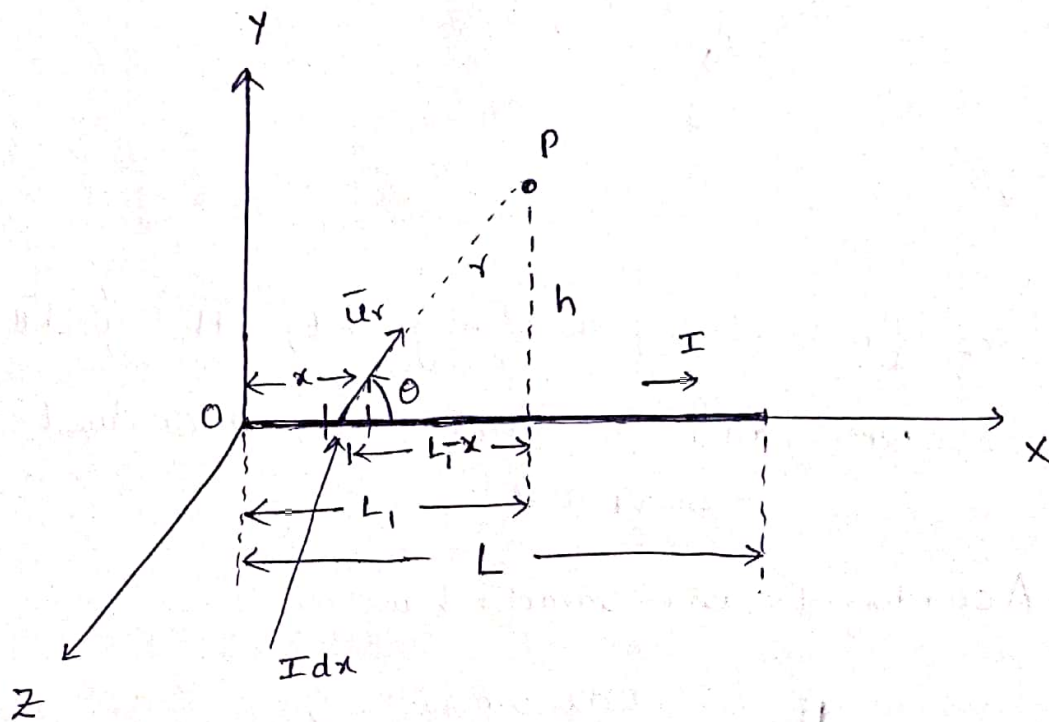
→ Field is directed perpendicular to the  $xy$ -plane.  
i.e., along  $z$ -axis

$$\vec{H} = \hat{k} \cdot \frac{I}{4\pi a^2} \oint dl$$

$$= \hat{k} \cdot \frac{I}{4\pi a^2} (2\pi a)$$

$$\boxed{\vec{H} = \frac{I}{2a} \hat{k}}$$

(2) Field Intensity at a point 'p' due to a straight Conductor carrying a current, I :



- Let 'p' be any point distant 'h' from the straight Conductor in xy-plane .
- Let us take the conductor to be along the x-axis from O; length of the Conductor, L .
- Consider Any Current element "Idx" at a distance x from O and let its distance to p be 'r'.

According to Biot-Savart's law,

$$dH_p = \frac{I dx}{4\pi r^2} \hat{i} \times \hat{r}$$

$$dH_p = \frac{I dx \sin \theta}{4\pi r^2} \hat{k} \quad \left[ \because \hat{i} \times \hat{r} = (\sin \theta) \hat{k} \right]$$

Total field intensity at 'p' is

$$H_p = \int dH_p$$

$$H_p = \hat{k} \frac{I}{4\pi} \int \frac{\sin \theta}{r^2} dx$$

From the diagram

$$\tan \theta = \frac{h}{L_1 - x}$$

$$\Rightarrow \cot \theta = \frac{L_1 - x}{h}$$

$$\Rightarrow L_1 - x = h \cot \theta$$

$$-dx = -h \operatorname{cosec}^2 \theta d\theta$$

$$\boxed{dx = h \operatorname{cosec}^2 \theta d\theta}$$

$$\sin \theta = \frac{h}{r}$$

$$\Rightarrow \operatorname{cosec} \theta = \frac{r}{h}$$

$$\Rightarrow \boxed{r = h \operatorname{cosec} \theta}$$

Substitute  $dx$  &  $r$  in the above equation

$$H_p = \hat{k} \frac{I}{4\pi} \int \frac{\sin \theta}{h \operatorname{cosec} \theta} \cdot h \operatorname{cosec}^2 \theta d\theta$$

$$= \hat{k} \frac{I}{4\pi h} \int \sin \theta d\theta$$

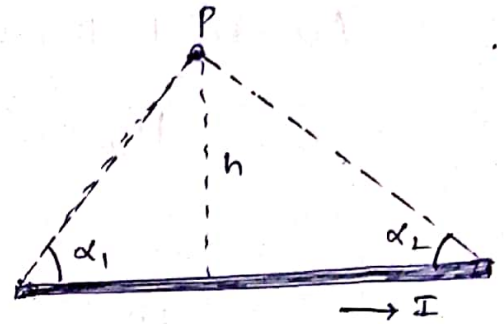
$$= \hat{k} \frac{I}{4\pi h} \left[ -\cos \theta \right]_{\theta \text{ for } x=0}^{\theta \text{ for } x=L}$$

$$H_p = \hat{k} \frac{I}{4\pi h} \left[ -\cos\theta \right]_{\alpha_1}^{\pi-\alpha_2}$$

$$H_p = \hat{k} \frac{I}{4\pi h} \left[ -\cos(\pi-\alpha_2) + \cos\alpha_1 \right]$$

$$H_p = \hat{k} \frac{I}{4\pi h} \left[ \cos\alpha_1 + \cos\alpha_2 \right]$$

$$H_p = \frac{I}{4\pi h} \left[ \cos\alpha_1 + \cos\alpha_2 \right] \hat{k}$$



NOTE: For infinite long straight conductor carrying current  $I$ , the field intensity at  $P$  is given by

$$H_p = \frac{I}{2\pi h} \hat{k}$$

$$[\because \alpha_1 = \alpha_2 = 0]$$

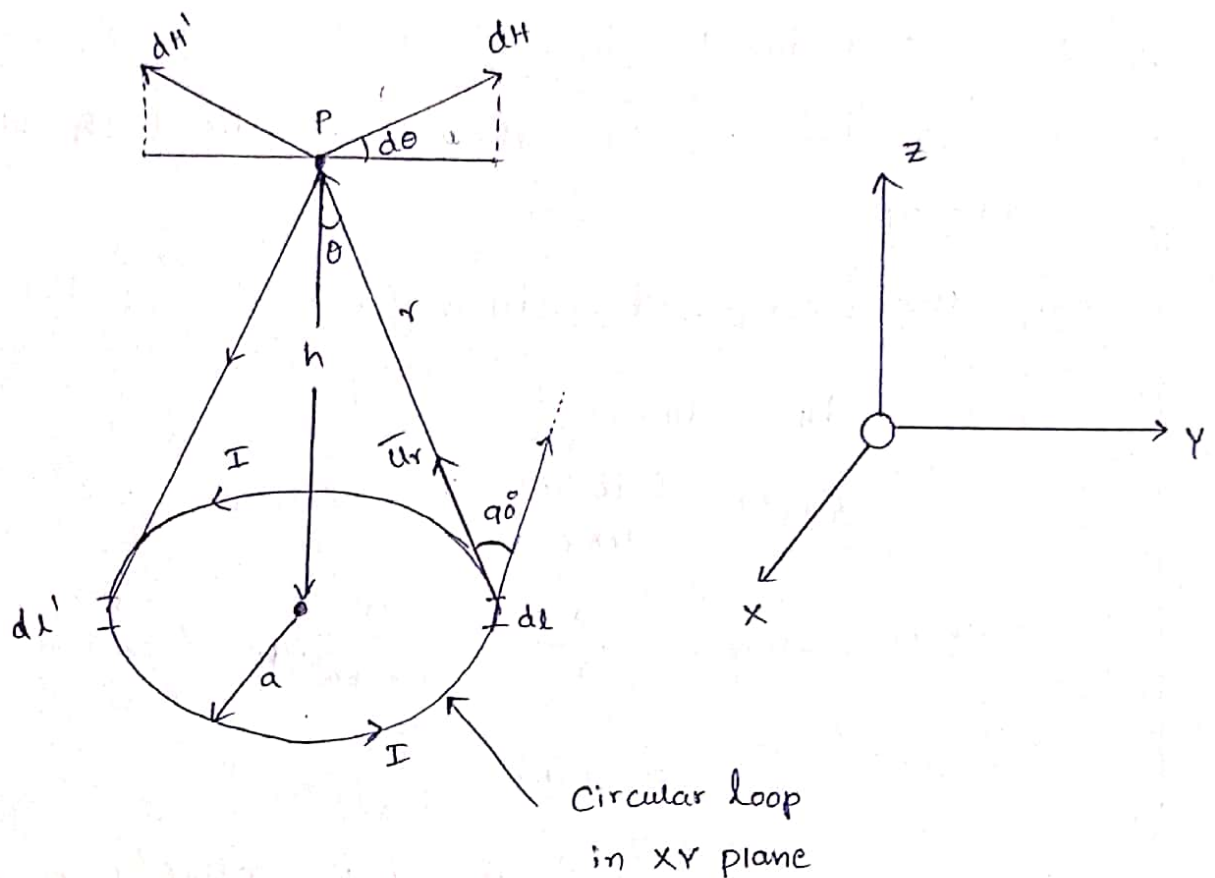
The corresponding flux density expressions are

$$B_p = \frac{\mu_0 I}{4\pi h} \left[ \cos\alpha_1 + \cos\alpha_2 \right] \hat{k}$$

$$B_p = \frac{\mu_0 I}{2\pi h} \hat{k} \quad \text{— for infinite long conductor.}$$

(3) Field intensity  $H$  at a point 'P'

due to ~~the~~ Circular loop carrying Current  $I$  :



→ Consider two diametrically opposite elements of the wire loop  $dl$  and  $dl'$ .

The field intensity at  $P$  distant  $r$  from the Current element  $Idl$  is given by

$$dH = \frac{Idl \times \bar{ur}}{4\pi r^2}$$

As the Vectors  $d\bar{l}$  and  $\bar{ur}$  are perpendicular,

$$dH = \frac{Idl}{4\pi r^2}$$

→ The field is Oriented at an angle  $\theta$  to the plane of loop.

→ The diametrically opposite element  $Idl'$  will also produce a field of magnitude equal to  $dH$ ; but its Component parallel to the plane of the loop, though equal is oppositely directed to the field due to element  $Idl$ .

→ However, the Components along  $z$ -axis due to the elements add up.

The  $z$ -Component of  $dH$  is given by

$$dH_z = dH \sin \theta$$

$$dH_z = \frac{Idl \sin \theta}{4\pi r^2}$$

Where  $\sin \theta = \frac{a}{r} = \frac{a}{(a^2 + h^2)^{1/2}}$

$$r^2 = a^2 + h^2$$

The resultant field intensity at the point 'P' is given

$$H_p = \oint dH_z$$

$$= \oint \frac{Idl}{4\pi (a^2 + h^2)^{3/2}} \cdot \frac{a}{(a^2 + h^2)^{1/2}}$$

$$= \frac{Ia}{4\pi (a^2 + h^2)^{3/2}} \oint dl$$

$$H_p = \frac{Ia}{2\pi (a^2 + h^2)^{3/2}} (2\pi a) \quad \left[ \because \oint dl = \text{length of the wire loop} \right]$$

$$H_p = \frac{Ia^2}{2(a^2 + h^2)^{3/2}} \hat{k}$$

→  $H_p$  is directed along  $z$ -axis

**Note** If  $h=0$ ,  $p$  coincides with  $O$ , the centre of the wire loop,

$$\vec{H} = \frac{Ia^2}{2a^3} \hat{k} = \frac{I}{2a} \hat{k}$$

(4) Field  $\vec{B}$  at any point along the axis of a Solenoid :

Solenoid:

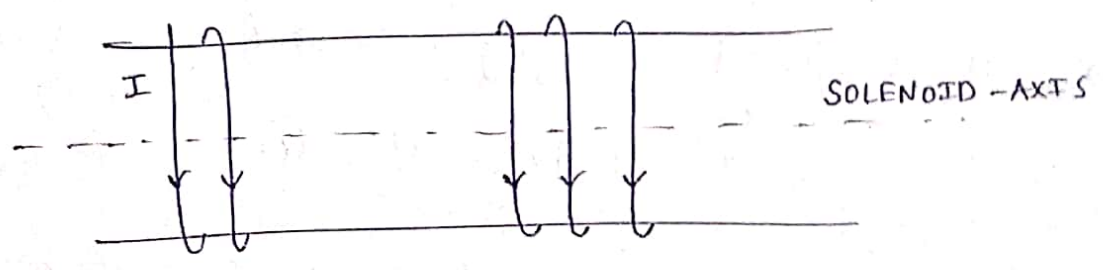
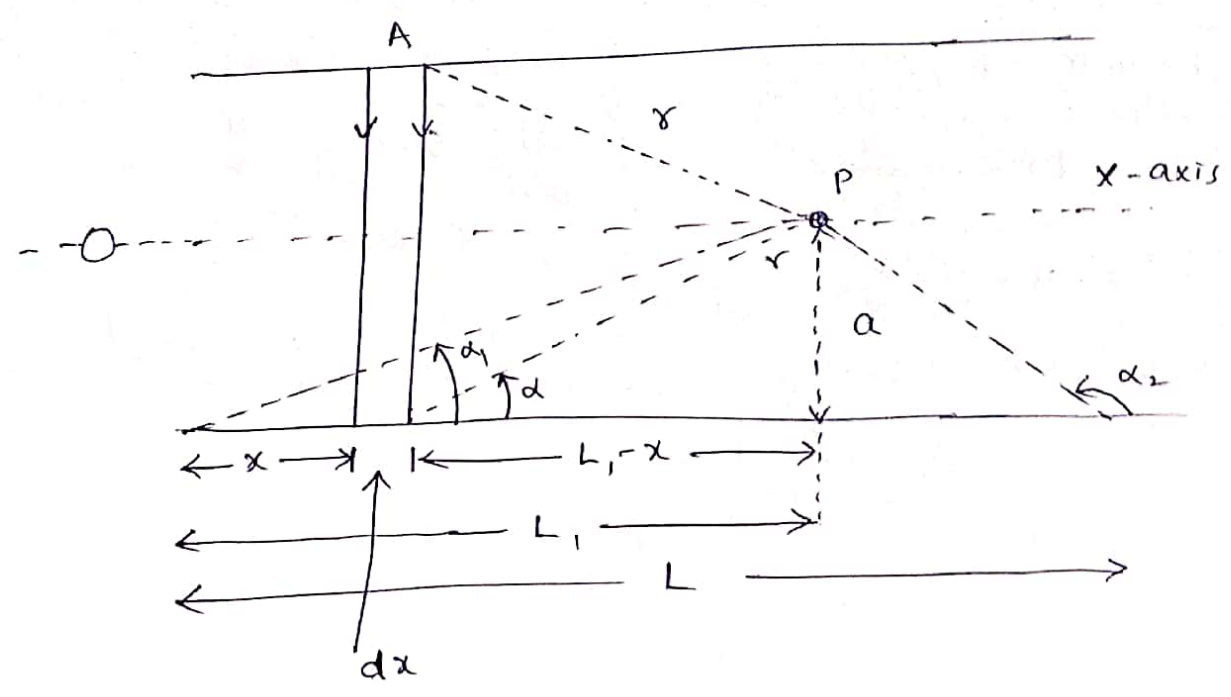


Fig: Solenoid.

"A solenoid is a cylindrically shaped coil consisting of a large number of closely spaced turns of insulated wire wound usually on a non-magnetic frame"



→ Let the Solenoid have  $N$  turns uniformly distributed over a length  $L$  and mean radius of the coil  $= a$ .

→ For ' $L$ ' length, the no. of turns  $= N$

For unit length, the no. of turns  $= \frac{N}{L}$

For ' $dx$ ' length, the no. of turns  $= \frac{N}{L} dx$

→ As the current is  $I$ , we can consider that the current in the coil produces a current sheet with a linear current density

$$\lambda = \frac{NI}{L}.$$

→ The length  $dx$  carrying a current

$$I' = \lambda dx = \frac{NI}{L} dx.$$

→ Hence, the field  $d\vec{B}$  due to the current sheet of length  $dx$  is

$$d\vec{B} = \frac{\mu_0 I' a^2}{2x^3} \hat{i}$$

$$d\vec{B} = \hat{i} \frac{\mu_0 I a^2}{2x^3} \frac{N}{L} dx.$$

From the figure

$$\tan \alpha = \frac{a}{L-x}$$

$$\Rightarrow \cot \alpha = \frac{L-x}{a}$$

$$\Rightarrow L-x = a \cot \alpha$$

$$\boxed{dx = a \operatorname{cosec}^2 \alpha d\alpha}$$

$$\sin \alpha = \frac{a}{r}$$

$$\Rightarrow \operatorname{cosec} \alpha = \frac{r}{a}$$

$$\Rightarrow \boxed{r = a \operatorname{cosec} \alpha}$$

$$d\vec{B} = \hat{i} \frac{\mu_0 I a^2}{2a^2 \csc^3 \alpha} \cdot \frac{N}{L} a \csc \alpha d\alpha$$

$$d\vec{B} = \hat{i} \frac{\mu_0 N I}{2L} \sin \alpha d\alpha$$

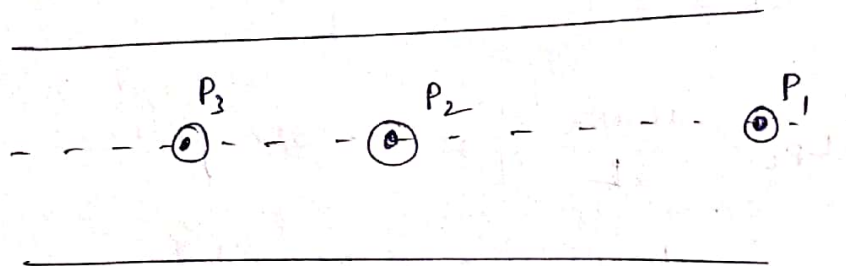
The resultant field at 'p' is

$$\vec{B} = \int_{\alpha_1}^{\alpha_2} d\vec{B} = \int_{\alpha_1}^{\alpha_2} \hat{i} \frac{\mu_0 N I}{2L} \sin \alpha d\alpha$$

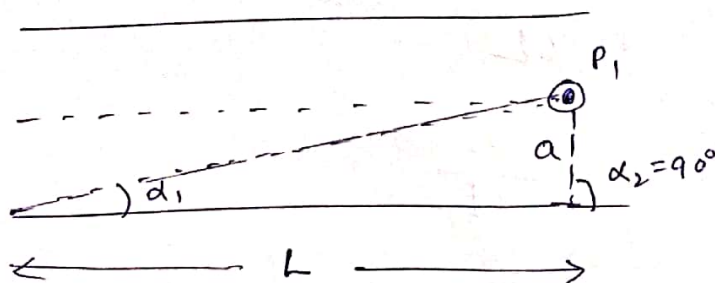
$$\vec{B} = \frac{\mu_0 N I}{2L} [-\cos \alpha]_{\alpha_1}^{\alpha_2} \hat{i}$$

$$\boxed{\vec{B} = \frac{\mu_0 N I}{2L} [\cos \alpha_1 - \cos \alpha_2] \hat{i}}$$

Let us consider three particular locations of p.



Case(i): Let p be at one of the ends of the solenoid.



$$\cos \alpha_1 = \frac{L}{\sqrt{L^2 + a^2}}$$

If  $L \gg a$

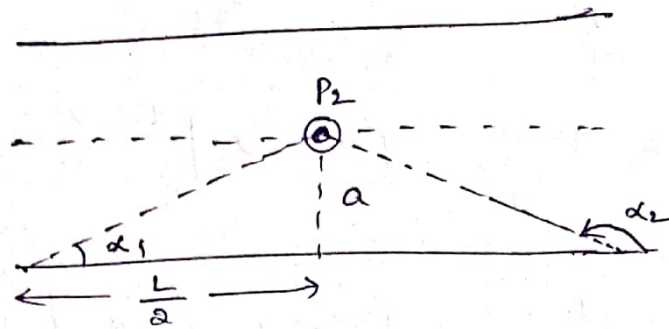
$$\cos \alpha_1 = 1$$

$$\cos \alpha_2 = \cos 90^\circ = 0$$

$$B_{P_1} = \frac{\mu_0 N I}{2L} [1 - 0]$$

$$B_{P_1} = \frac{\mu_0 N I}{2L} \hat{i}$$

Case (2): Let 'p' be at the centre of the solenoid



$$\cos \alpha_1 = \frac{L/2}{\sqrt{(L/2)^2 + a^2}}$$

If  $L/2 \gg a$

$$\cos \alpha_1 = 1$$

$$\cos(\pi - \alpha_2) = \cos \alpha_1$$

$$\Rightarrow \cos \alpha_2 = -\cos \alpha_1$$

$$B_{P_2} = \frac{\mu_0 N I}{2L} [\cos \alpha_1 - \cos \alpha_2] \hat{i}$$

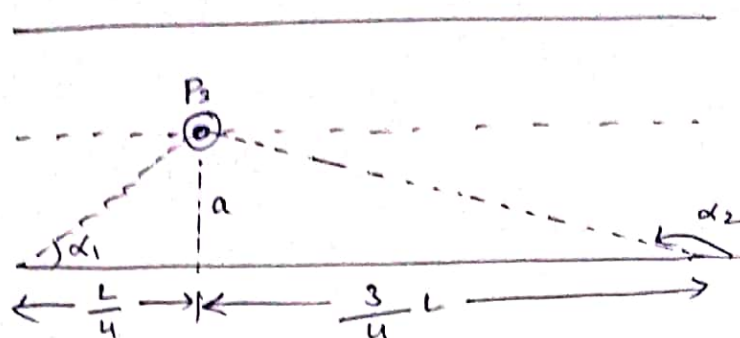
$$= \frac{\mu_0 N I}{2L} [\cos \alpha_1 + \cos \alpha_1] \hat{i}$$

$$= \frac{\mu_0 N I}{2L} 2 \cos \alpha_1 \hat{i}$$

$$= \frac{\mu_0 N I}{L} (1) \hat{i}$$

$$B_{P_2} = \frac{\mu_0 N I}{L} \hat{i}$$

Case (3): Let 'p' be a point on the axis, midway between one end and centre of the solenoid.



$$\cos \alpha_1 = \frac{L/4}{\sqrt{(L/4)^2 + a^2}}$$

$$= \frac{L}{\sqrt{L^2 + 16a^2}}$$

$$\cos(\pi - \alpha_2) = \frac{3/4 L}{\sqrt{(3/4 L)^2 + a^2}}$$

If  $\frac{3}{4} L \gg a$ .

$$\cos(\pi - \alpha_2) = 1$$

$$-\cos \alpha_2 = 1$$

$$\boxed{\cos \alpha_2 = -1}$$

$$B_{P_3} = \frac{\mu_0 N I}{2L} [\cos \alpha_1 - \cos \alpha_2]$$

$$B_{P_3} = \frac{\mu_0 N I}{2L} \left[ 1 + \frac{L}{\sqrt{L^2 + 16a^2}} \right] \hat{i}$$

Graph:

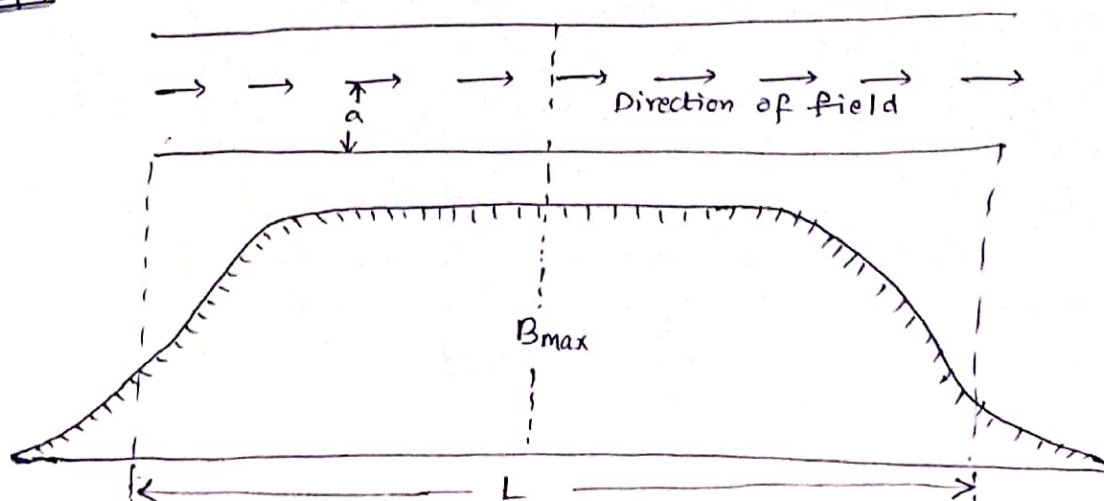


Fig: Variation of B along the axis of a long Slender Solenoid.

## Ampere's Circuital Law (Ampere's Work Law)

- When the magnetic field has some form of symmetry, the magnetic flux density can be determined with the application of law known as Ampere's Law.
- In Electrostatics, Complex problems can be Solved using a law called Gauss's law.  
Gauss's Law is useful to obtain  $\vec{E}$ .
- Similarly, in Magnetostatics, Complex problems can be Solved using a law called Ampere's circuital Law.

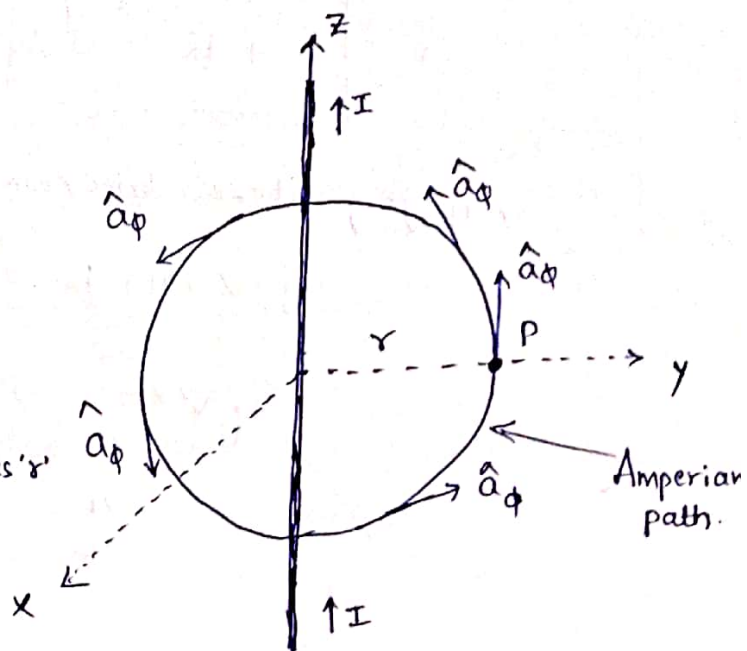
### Statement:

Ampere's circuit law states that the line integral of  $\vec{H}$  around a closed path is the same as the net current,  $I_{enc}$  enclosed by the path.

$$\oint_L \vec{H} \cdot d\vec{l} = I_{enc}$$

### Proof:

- Consider a long straight Conductor carrying 'I' placed along z-axis.
- Consider a closed Circular path or Amperian path of radius 'r' which encloses the straight Conductor carrying current, 'I'.



→ Consider  $d\vec{l}$  at point 'p' which is in  $\hat{a}_\phi$  direction, tangential to circular path at point 'p'.

From Biot-Savart's law,

∴  $\vec{H}$  due to infinitely long conductor is

$$\vec{H} = \frac{I}{2\pi r} \hat{a}_\phi$$

→ In cylindrical Co-ordinate system, the  $d\vec{l}$  in  $\hat{a}_\phi$  direction

$$\boxed{d\vec{l} = r d\phi \hat{a}_\phi}$$

$$\oint \vec{H} \cdot d\vec{l} = \oint \frac{I}{2\pi r} \hat{a}_\phi \cdot r d\phi \hat{a}_\phi$$

$$= \int_{\phi=0}^{2\pi} \frac{I}{2\pi} \cdot d\phi$$

$$= \frac{I}{2\pi} [\phi]_0^{2\pi}$$

$$= \frac{I}{2\pi} [2\pi]$$

$$= I_{enc}$$

$$\Rightarrow \boxed{\oint \vec{H} \cdot d\vec{l} = I_{enc}}$$

← Ampere's Law in integral form

Applying Stokes's theorem to the L.H.S

$$\int_s (\nabla \times \vec{H}) \cdot d\vec{s} = \int_s \vec{J} \cdot d\vec{s}$$

$$\boxed{\nabla \times \vec{H} = \vec{J}}$$

← Ampere's Law in differential or point form

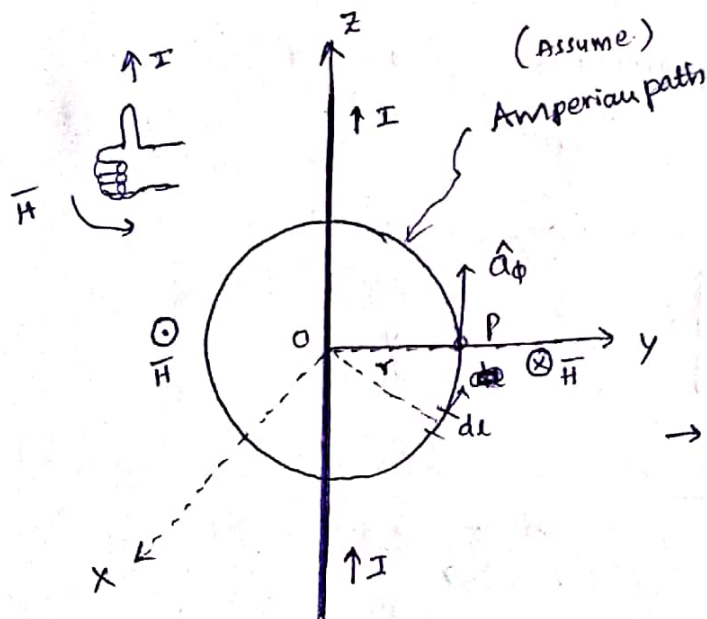
↑ Maxwell's 3<sup>rd</sup> equation.

**NOTE** Since,  $\nabla \times \vec{H} \neq 0$ ; a magnetostatic field is not conservative.

# Applications of Ampere's Circuit Law:

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## (1) $\vec{H}$ due to Infinitely long Straight Conductor:



According to Ampere's law

$$\oint \vec{H} \cdot d\vec{l} = I_{enc}$$

→ Consider closed path  $\approx$  Amperian path  
which shows that  $\vec{H}$  is constant  
as  $r$  is constant.

$$\vec{H} = H_r \hat{a}_r + H_\phi \hat{a}_\phi + H_z \hat{a}_z$$

$$\vec{H} = H_\phi \hat{a}_\phi \quad [r \text{ is constant, } z=0 \text{ for point P}]$$

$d\vec{l} \rightarrow$  elementary length  $\Rightarrow$  a Cylindrical Coordinate System

$$d\vec{l} = r \cdot d\phi \hat{a}_\phi$$

$$\vec{H} \cdot d\vec{l} = (H_\phi \hat{a}_\phi) (r d\phi \hat{a}_\phi) = H_\phi \cdot r \cdot d\phi$$

According to Ampere's Circuit Law

$$\oint \vec{H} \cdot d\vec{l} = I_{enc}$$

$$\int_{\phi=0}^{2\pi} H_\phi \cdot r \cdot d\phi = I \Rightarrow H_\phi \cdot r \cdot \int_0^{2\pi} d\phi = I$$

$$\Rightarrow H_\phi \cdot r \cdot [\phi]_0^{2\pi} = I$$

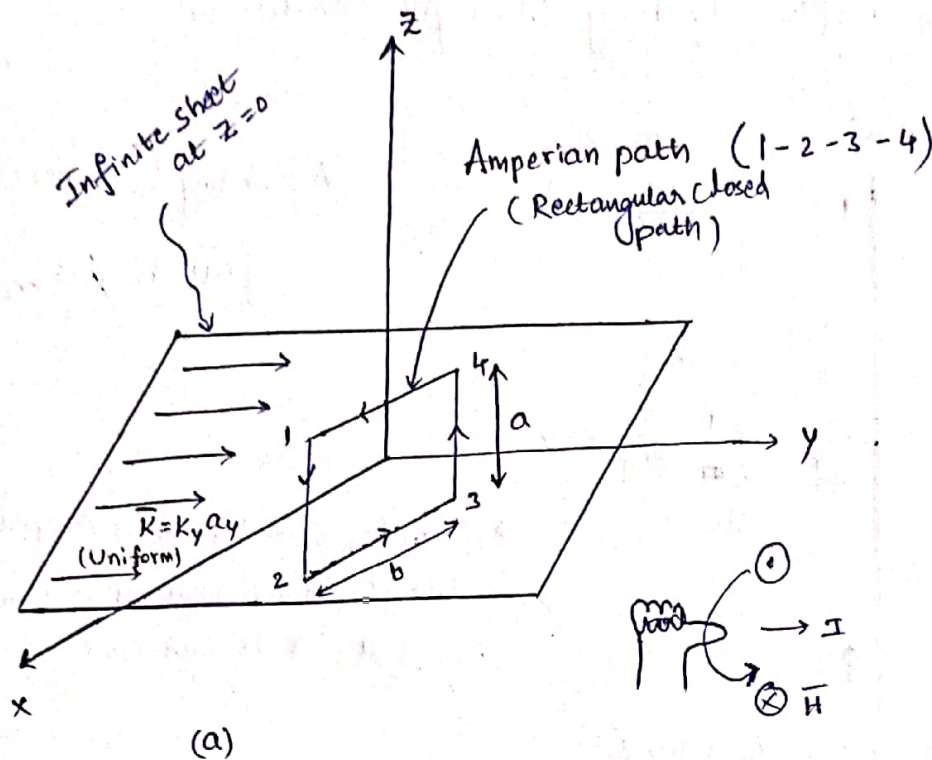
$$\Rightarrow H_\phi \cdot r \cdot [2\pi] = I$$

$$\Rightarrow H_\phi = \frac{I}{2\pi r}$$

$$\vec{H} = H_\phi \hat{a}_\phi = \frac{I}{2\pi r} \hat{a}_\phi$$

$$\boxed{\vec{H} = \frac{I}{2\pi r} \hat{a}_\phi \quad \text{A/m}}$$

(2)  $\vec{H}$  due to Infinite sheet of Current :



$K_y = \frac{I}{b} = \text{Surface current density.}$

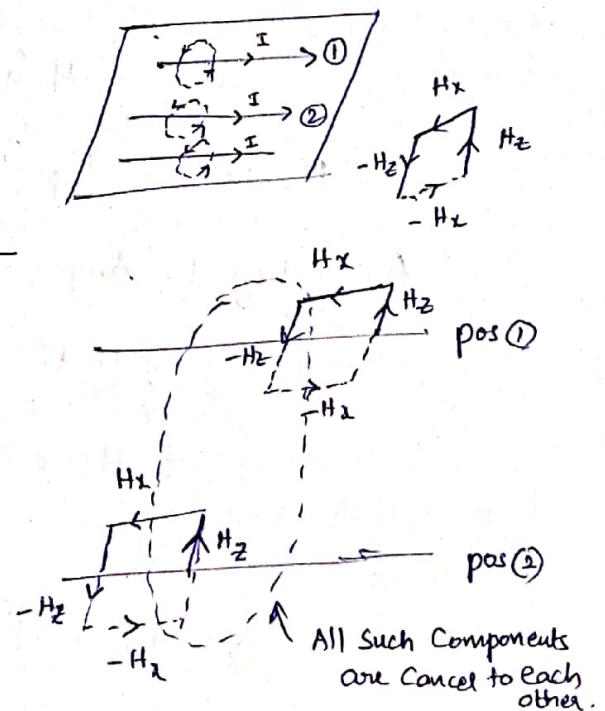
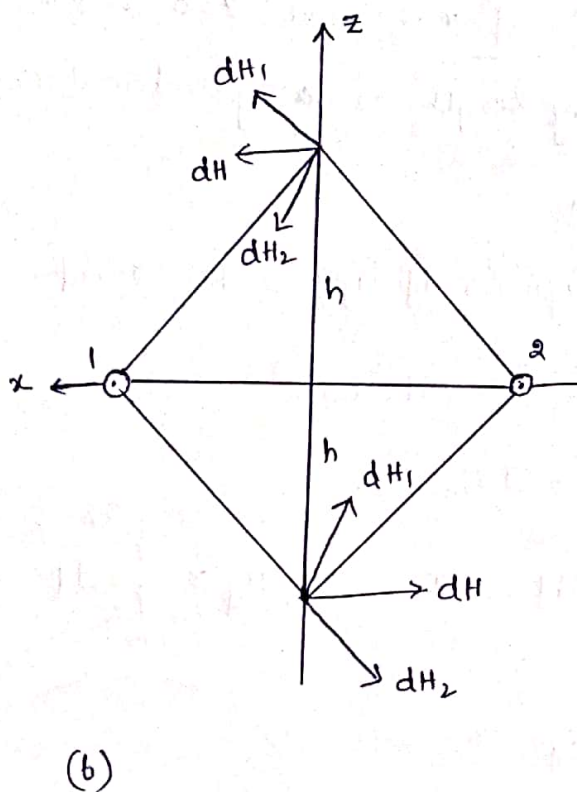


Fig: Application of Ampere's Law to an infinite sheet

(a) Closed path 1-2-3-4-1

(b) Symmetrical pair of current ~~elements~~ filaments with Current along  $\hat{a}_y$ .

## Applying Ampere's Circuit law

$$\oint \vec{H} \cdot d\vec{l} = I_{enc}$$

- Consider an infinite ~~sheet~~ current sheet in the  $z=0$  plane.
  - As current is flowing in  $y$ -direction,  $\vec{H}$  cannot have Component in  $y$ -direction.
  - $\vec{H}$  along the  $z$ -axis is cancelled due to symmetry.
- So,  $\vec{H}$  has only Component in  $x$ -direction.

$$\begin{aligned}\vec{H} &= H_x \vec{a}_x \text{ for } z > 0 \\ &= -H_x \vec{a}_x \text{ for } z < 0\end{aligned}$$

For path 1-2,  $d\vec{l} = dz(-\vec{a}_z)$

For path 3-4,  $d\vec{l} = dz \vec{a}_z$

$$\begin{aligned}\oint \vec{H} \cdot d\vec{l} &= \left( \int_1^2 + \int_2^3 + \int_3^4 + \int_4^1 \right) \vec{H} \cdot d\vec{l} \\ &= -H_x(-a) + (-H_x)(-b) + (H_x)(a) + H_x(b) \\ &= 2H_x b \quad [H_z = -H_z]\end{aligned}$$

$$\begin{aligned}\int_1^2 \vec{H} \cdot d\vec{l} + \int_3^4 \vec{H} \cdot d\vec{l} &= \int_1^2 -H_x \vec{a}_x \cdot dz(-\vec{a}_z) + \int_3^4 H_x \vec{a}_x \cdot dz \vec{a}_z \\ &= 0 + 0 \\ &= 0\end{aligned}$$

$[\because \vec{a}_x \cdot \vec{a}_z = 0]$

For path 2-3

$$\begin{aligned}\int_2^3 \vec{H} \cdot d\vec{l} &= \int_2^3 -H_x \vec{a}_x \cdot dx \vec{a}_x (-\vec{a}_x) \\ &= H_x \int_2^3 dx = b \cdot H_x\end{aligned}$$

For path 4-1

$$\begin{aligned}\int_4^1 \vec{H} \cdot d\vec{l} &= \int_4^1 H_x \vec{a}_x \cdot dx \vec{a}_x \\ &= H_x \int_4^1 dx = b H_x\end{aligned}$$

$$\oint \mathbf{H} \cdot d\mathbf{l} = \int_1^2 \mathbf{H} \cdot d\mathbf{l} + \int_2^3 \mathbf{H} \cdot d\mathbf{l} + \int_3^4 \mathbf{H} \cdot d\mathbf{l} + \int_4^1 \mathbf{H} \cdot d\mathbf{l}$$

$$= 0 + b \cdot H_x + 0 + b H_x$$

$$= 2b H_x$$

→ The current flowing across the distance 'b' is  $K_y b$

$$I_{enc} = K_y b$$

→ According to Ampere's law

$$\oint \mathbf{H} \cdot d\mathbf{l} = I_{enc}$$

$$2b H_x = K_y b$$

$$\Rightarrow \boxed{H_x = \frac{1}{2} K_y}$$

$$\text{Then, } \mathbf{H} = \frac{1}{2} K_y \mathbf{\bar{a}_x} \text{ for } z > 0$$

$$= -\frac{1}{2} K_y \mathbf{\bar{a}_x} \text{ for } z < 0$$

In general, for an infinite sheet of current density  $K \text{ A/m}$ ,

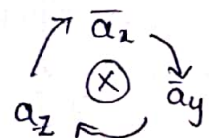
$$\boxed{\mathbf{H} = \frac{1}{2} \mathbf{K} \times \mathbf{\bar{a}_n}}$$

$$\text{Here } \mathbf{\bar{a}_n} = \mathbf{\bar{a}_z}$$

$$\mathbf{K} = K_y \mathbf{\bar{a}_y}$$

$$\mathbf{K} \times \mathbf{\bar{a}_n} = K_y (\mathbf{\bar{a}_y} \times \mathbf{\bar{a}_z}) = K_y \mathbf{\bar{a}_x}$$

where  $\mathbf{\bar{a}_n}$  is a unit normal vector directed from the current sheet to the point of interest.



### (3) $\vec{H}$ due to Infinitely Long Co-axial Cable

RNL Chanay  
(14)

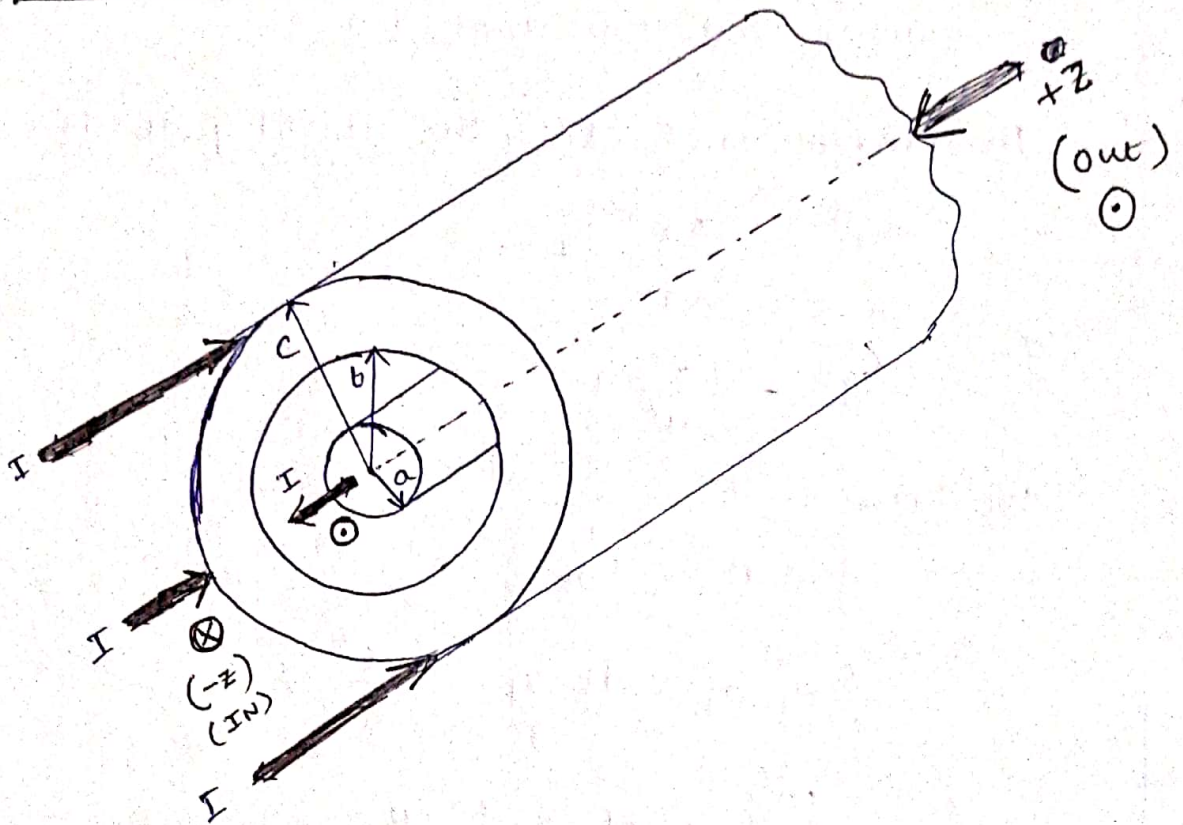
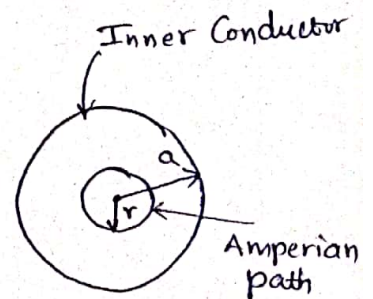


Fig: ~~Consider~~ a Co-axial Cable (Two Concentric cylinders)

→ Apply Ampere's circuit law along Amperian path for each possibility.

Region (1): Within the inner conductor,  $r < a$  ( $0 \leq r \leq a$ )

→ Within the inner conductor, Consider an Amperian path having radius  $r < a$



According to Ampere's Circuital Law

$$\oint \vec{H} \cdot d\vec{l} = I'$$

where  $I'$  is the current enclosed by the closed path.

$$\vec{H} = H_\phi \cdot \vec{a}_\phi$$

$$d\vec{l} = r \cdot d\phi \cdot \vec{a}_\phi$$

Area of the enclosed cross section is  $\pi r^2$

→ The current,  $I$  which is flowing through inner conductor area,  $\pi a^2$ .

The current enclosed by the closed path is

$$I' = \frac{\pi r^2}{\pi a^2} I$$

$$I' = \frac{r^2}{a^2} I$$

We know

$$\oint \mathbf{H} \cdot d\mathbf{l} = I'_{enc}$$

$$\oint H_\phi \cdot \bar{a}_\phi \cdot r \cdot d\phi \cdot \bar{a}_\phi = \frac{r^2}{a^2} I$$

$$\int_{\phi=0}^{2\pi} H_\phi \cdot r \cdot d\phi = \frac{r^2}{a^2} I$$

$$H_\phi \cdot r \cdot [\phi]_0^{2\pi} = \frac{r^2}{a^2} I$$

$$H_\phi \cdot (2\pi) = \frac{r}{a^2} I$$

$$H_\phi = \frac{Ir}{2\pi a^2}$$

$$\boxed{\bar{\mathbf{H}} = \bar{H}_\phi \cdot \bar{a}_\phi = \frac{Ir}{2\pi a^2} \bar{a}_\phi} \quad \text{A/m}$$

Region(2): With in  $a \leq r \leq b$

$$\oint \mathbf{H} \cdot d\mathbf{l} = I$$

$$\int_{\phi=0}^{2\pi} H_\phi \cdot \bar{a}_\phi \cdot r \cdot d\phi \cdot \bar{a}_\phi = I$$

$$H_\phi \cdot r \cdot [\phi]_0^{2\pi} = I$$

$$\Rightarrow H_{\phi} \cdot r \cdot (2\pi) = I$$

$$\Rightarrow H_{\phi} = \frac{I}{2\pi r}$$

$$\vec{H} = H_{\phi} \cdot \vec{a}_{\phi} = \frac{I}{2\pi r} \vec{a}_{\phi}$$

$$\boxed{\vec{H} = \frac{I}{2\pi r} \vec{a}_{\phi}} \quad \text{A/m}$$

Region(3): With in Outer Conductor,  $b \leq r \leq c$

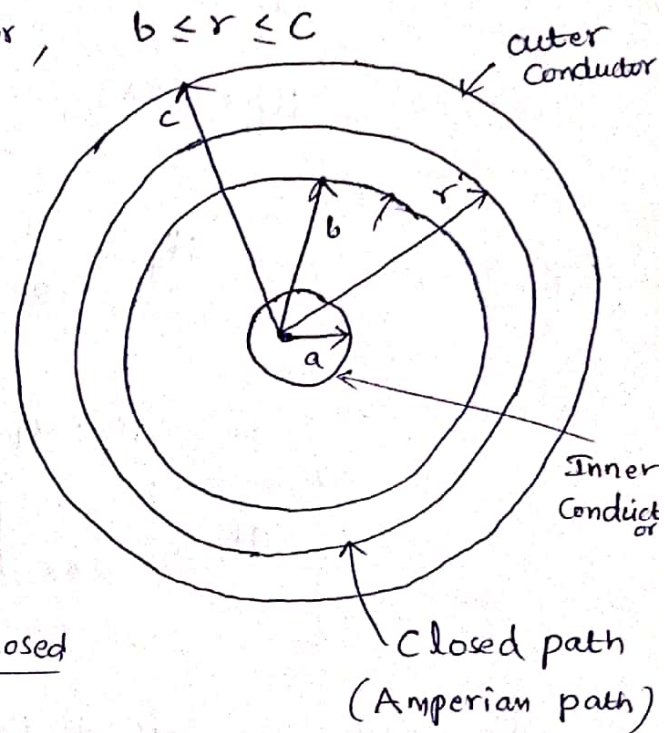
Current in Outer Conductor enclosed

$$I' = \frac{\cancel{\pi} (r^2 - b^2)}{\cancel{\pi} (c^2 - b^2)} (-I)$$

$$I' = - \frac{(r^2 - b^2)}{(c^2 - b^2)} I$$

Current in inner Conductor enclosed

$$I'' = I$$



Total Current enclosed by the closed path is

$$I_{enc} = I' + I''$$

$$= - \frac{(r^2 - b^2)}{(c^2 - b^2)} I + I$$

$$= I \left[ 1 - \frac{(r^2 - b^2)}{(c^2 - b^2)} \right] = I \left[ \frac{\cancel{c^2} - \cancel{b^2} - r^2 + \cancel{b^2}}{c^2 - b^2} \right]$$

$$I_{enc} = I \left[ \frac{c^2 - r^2}{c^2 - b^2} \right]$$

Apply Ampere's Law

$$\oint \mathbf{H} \cdot d\mathbf{l} = I_{enc}$$

$$\oint \mathbf{H} \cdot d\mathbf{l} = \int_0^{2\pi} (H_\phi \cdot \bar{a}_\phi) (r \cdot d\phi \cdot \bar{a}_\phi) = H_\phi \cdot r [\phi]_0^{2\pi} \\ = H_\phi \cdot r (2\pi)$$

$$\Rightarrow \oint \mathbf{H} \cdot d\mathbf{l} = I_{enc}$$

$$H_\phi \cdot r \cdot (2\pi) = I \left[ \frac{c^2 - r^2}{c^2 - b^2} \right]$$

$$H_\phi = \frac{I}{2\pi r} \left[ \frac{c^2 - r^2}{c^2 - b^2} \right]$$

$$\bar{\mathbf{H}} = H_\phi \cdot \bar{\mathbf{a}}_\phi$$

$$\boxed{\bar{\mathbf{H}} = \frac{I}{2\pi r} \left[ \frac{c^2 - r^2}{c^2 - b^2} \right] \bar{\mathbf{a}}_\phi} \quad \text{A/m.}$$

Region (4): Outside the Cable,  $r > c$

→ consider a the closed path having radius  $r > c$ ,

Such that it closes both the conductors.

$$\text{so, } I_{enc} = +I - I = 0$$

Apply Ampere's Law

$$\oint \mathbf{H} \cdot d\mathbf{l} = I_{enc} = 0$$

$$\boxed{\bar{\mathbf{H}} = 0} \quad \text{A/m}$$

$$H = \begin{cases} \frac{I r}{2 \pi a^2} \bar{a}_\phi & \text{for } 0 \leq r \leq a \\ \frac{I}{2 \pi r} \bar{a}_\phi & \text{for } a \leq r \leq b \\ \frac{I}{2 \pi r} \left[ \frac{c^2 - r^2}{c^2 - b^2} \right] \bar{a}_\phi & \text{for } b \leq r \leq c \\ 0 & \text{for } r > c \end{cases}$$

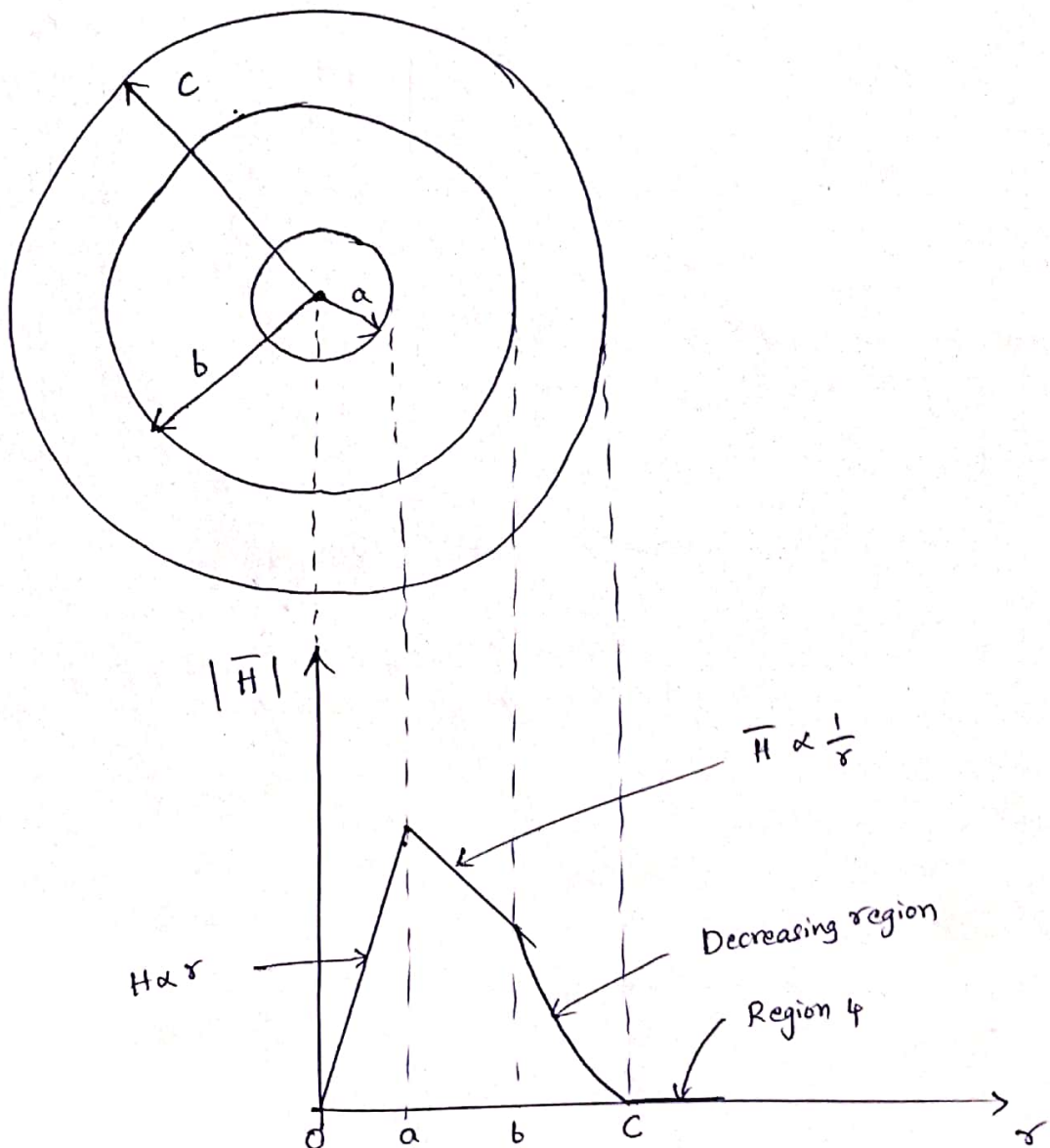


Fig: plot of  $H$  against  $r$

## MAGNETIC FLUX DENSITY - MAXWELL'S EQUATION

RNL Chan

(17)

The magnetic flux density  $\vec{B}$  is similar to the electric flux density  $\vec{D}$ . As  $\vec{D} = \epsilon_0 \vec{E}$  in free space, the magnetic ~~field intensity~~ flux density  $\vec{B}$  is related to the magnetic field intensity  $\vec{H}$  according to

$$\boxed{\vec{B} = \mu \cdot \vec{H}}$$

where  $\mu$  = permeability of medium  
 $= \mu_0 \mu_r$

$\mu_0$  = permeability of free space  
 $= 4\pi \times 10^{-7} \text{ H/m}$

$\mu_r$  = Relative permeability

~~The~~ For, free space, the  $\boxed{\vec{B} = \mu_0 \vec{H}}$   $[\because \mu_r = 1]$

→ The magnetic flux through a surface  $S$  is given by

$$\boxed{\phi = \int_S \vec{B} \cdot d\vec{s}} \quad \text{wb}$$

→ Magnetic flux density is measured in terms of  $\text{wb/m}^2$ .

→ In case of electrostatic field, we have seen that if the surface is a closed surface, the net flux passing through the surface is equal to the charge enclosed by the surface.

In case of magnetic field, isolated magnetic charge (i.e., pole) does not exist. Magnetic poles always occur in pair (as N-S).

→ For example, if we desire to have an isolated magnetic pole by dividing a magnetic bar successively into two, we end up with pieces each having north (N) and South (S) poles. This process could be continued ~~to~~ until the magnets are of atomic dimensions; still we will have N-S pair occurring together. This means that ~~the~~ it is impossible to separate the north pole from the south pole.

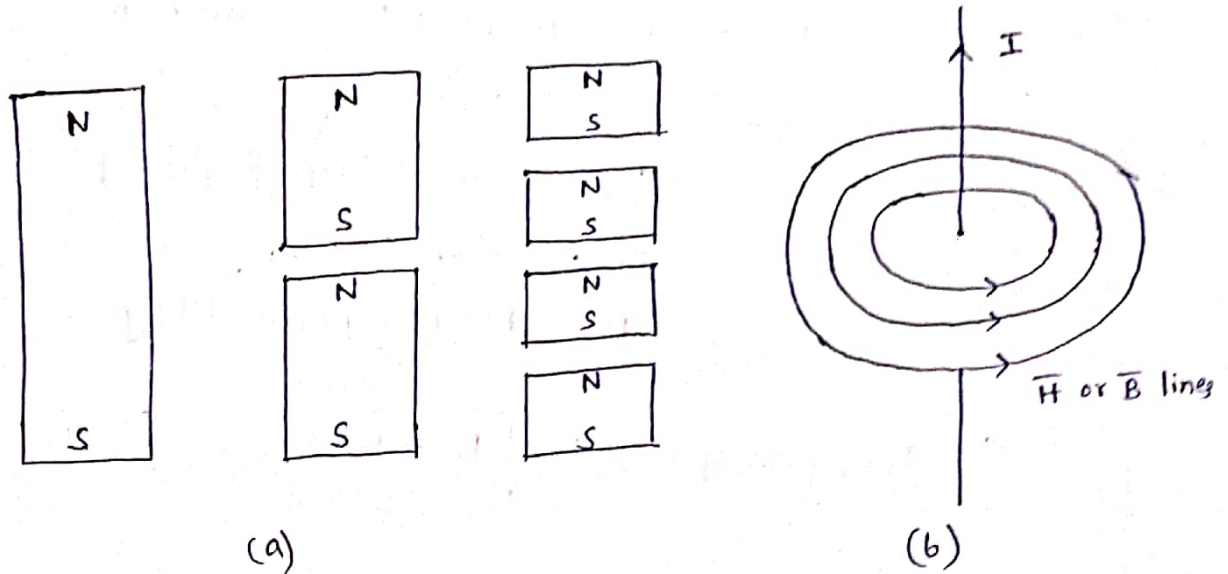
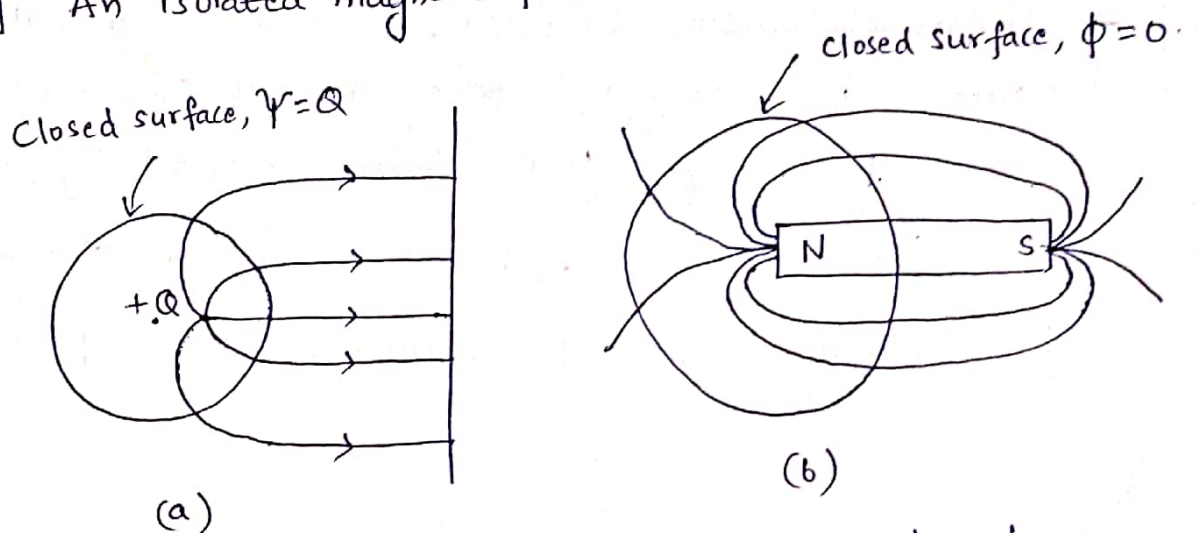


Fig: (a) Subdivision of a magnet  
(b) Magnetic field / flux lines of a straight current carrying conductor.

**NOTE** An isolated magnetic pole does not exist.



Fig(a): Flux leaving a closed surface due to (a) isolate electric charge  $\Psi = \oint_S \mathbf{D} \cdot d\mathbf{s} = Q_{enc}$  (b) magnetic charge,  $\phi = \oint_S \mathbf{B} \cdot d\mathbf{s} = 0$

Thus, the total flux through a closed surface in a magnetic field must be zero ; i.e

$$\boxed{\phi = \oint_s \mathbf{B} \cdot d\mathbf{s} = 0}$$

This equation is referred to as the law of Conservation of magnetic flux or Gauss's law for magnetic fields, just as  $\oint \mathbf{D} \cdot d\mathbf{s} = Q$  is Gauss's law for electrostatic fields.

→ Although the magnetostatic field is not conservative, magnetic flux is conserved.

By applying the divergence theorem to the above equation

$$\oint_s \mathbf{B} \cdot d\mathbf{s} = \int_v \nabla \cdot \mathbf{B} \cdot d\mathbf{v} = 0$$

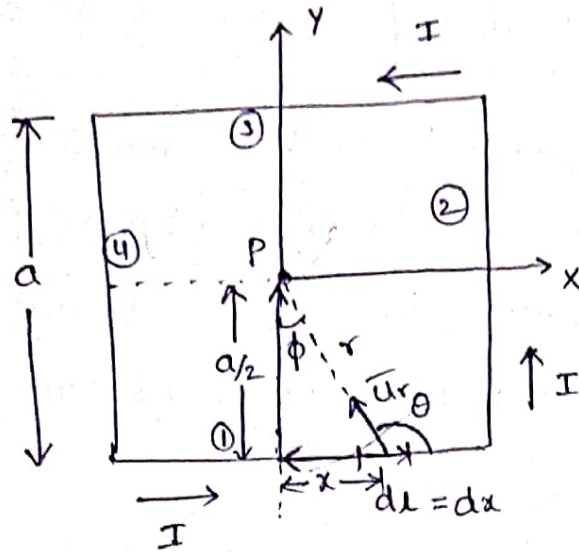
$$\boxed{\nabla \cdot \mathbf{B} = 0} \quad \leftarrow \text{Maxwell's fourth Equation}$$

→ The above equations shows that magnetostatic fields have no sources or sinks.

### MAXWELL'S EQUATIONS FOR STATIC FIELDS (static electric & magnetic fields)

| Differential (or) point form            | Integral Form                                                                | Remarks                                    |
|-----------------------------------------|------------------------------------------------------------------------------|--------------------------------------------|
| $\nabla \cdot \mathbf{D} = \rho_v$      | $\oint_s \mathbf{D} \cdot d\mathbf{s} = \int_v \rho_v \cdot d\mathbf{v}$     | Gauss's law                                |
| $\nabla \cdot \mathbf{B} = 0$           | $\oint_s \mathbf{B} \cdot d\mathbf{s} = 0$                                   | Non existence of magnetic monopole         |
| $\nabla \times \mathbf{E} = 0$          | $\oint_L \mathbf{E} \cdot d\mathbf{l} = 0$                                   | Conservative nature of electrostatic field |
| $\nabla \times \mathbf{H} = \mathbf{J}$ | $\oint_L \mathbf{H} \cdot d\mathbf{l} = \int_s \mathbf{J} \cdot d\mathbf{s}$ | Ampere's Law                               |

## Magnetic field $\vec{B}$ at the Centre of Square loop



By using Biot-Savart's Law

$$d\vec{B} = \frac{\mu_0 I}{4\pi} \left[ \frac{d\vec{l} \times \vec{u}_r}{r^2} \right]$$

$$= \frac{\mu_0 I}{4\pi} \left[ \frac{d\vec{l} \times \vec{r}}{r^3} \right] \quad \left[ \because \vec{u}_r = \frac{\vec{r}}{r} \right]$$

The total field,

$$\vec{B}_{\text{Total}} = \vec{B}_1 + \vec{B}_2 + \vec{B}_3 + \vec{B}_4$$

$$\vec{B}_{\text{Total}} = 4 \vec{B}_1$$

From the diagram,

$$d\vec{l} = dx \hat{i}$$

$$\sin\phi = \frac{x}{r}, \quad \cos\phi = \frac{a/2}{r}$$

$$\vec{r} = x(-\hat{i}) + \frac{a}{2} \hat{j}$$

$$\vec{r} = r \sin\phi (-\hat{i}) + r \cos\phi \hat{j}$$

$$\vec{r} = -r \sin\phi \hat{i} + r \cos\phi \hat{j}$$

$$d\vec{B} = \frac{\mu_0 I}{4\pi} \left[ \frac{d\vec{l} \times \vec{r}}{|\vec{r}|^3} \right]$$

$$d\vec{l} \times \vec{r} = dx \hat{i} \times [-|\vec{r}| \sin\phi \hat{i} + |\vec{r}| \cos\phi \hat{j}]$$

$$= [dx |\vec{r}| \cos\phi] \hat{k}$$

$$\left[ \begin{array}{l} \hat{i} \times \hat{i} = 0, \hat{j} \times \hat{j} = 0 \\ \hat{i} \times \hat{j} = \hat{k} \end{array} \right]$$

$$d\vec{B} = \frac{\mu_0 I}{4\pi} \left[ \frac{dx |\vec{r}| \cos\phi}{|\vec{r}|^3} \right] \hat{k}$$

$$d\vec{B} = \frac{\mu_0 I}{4\pi} \left[ \frac{dx \cos\phi}{|\vec{r}|^2} \right] \hat{k}$$

From the diagram

$$\tan\phi = \frac{x}{(a/2)}$$

$$\Rightarrow x = \frac{a}{2} \tan\phi$$

$$\Rightarrow dx = \left(\frac{a}{2}\right) \sec^2\phi \cdot d\phi$$

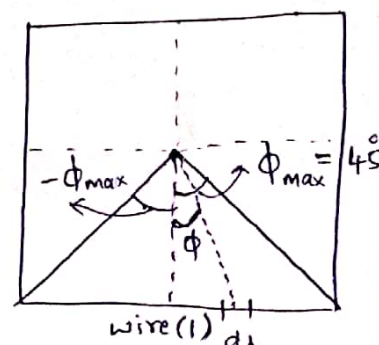
$$\Rightarrow dx = \left(\frac{a}{2}\right) \frac{1}{\cos^2\phi} \cdot d\phi$$

$$|\vec{r}| = \frac{a/2}{\cos\phi}$$

$$d\vec{B} = \frac{\mu_0 I}{4\pi} \left[ \left(\frac{a}{2}\right) \frac{1}{\cos^2\phi} \cdot d\phi \cdot \frac{\cos\phi}{\left(\frac{a/2}{\cos\phi}\right)^2} \right] \hat{k}$$

$$d\vec{B} = \frac{\mu_0 I}{4\pi} \left( \frac{1}{(a/2)} \right) \cos\phi \cdot d\phi \cdot \hat{k}$$

$$\vec{B}_1 = \int d\vec{B}_1 = \frac{\mu_0 I}{4\pi (a/2)} \int_{-\phi_{\max}}^{+\phi_{\max}} \cos\phi \cdot d\phi$$



$$\vec{B}_1 = \frac{\mu_0 I}{4\pi(a/2)} \left[ \sin\phi \right]_{-\phi_{\max}}^{\phi_{\max}} \hat{k}$$

$$= \frac{\mu_0 I}{4\pi(a/2)} \left[ \sin\phi_{\max} - \sin(-\phi_{\max}) \right] \hat{k}$$

$$= \frac{\mu_0 I}{4\pi(a/2)} \left[ 2\sin\phi_{\max} \right] \hat{k}$$

$$= \frac{\mu_0 I}{4\pi(a/2)} \times \cancel{2} \cdot \frac{\sqrt{2}}{\cancel{2}} \hat{k} \quad \left[ \because \sin 45^\circ = \frac{\sqrt{2}}{2} \right]$$

$$\vec{B}_1 = \frac{\mu_0 I}{4\pi(a/2)} \sqrt{2} \hat{k}$$

$$\vec{B}_{\text{Total}} = 4 \cdot \vec{B}_1$$

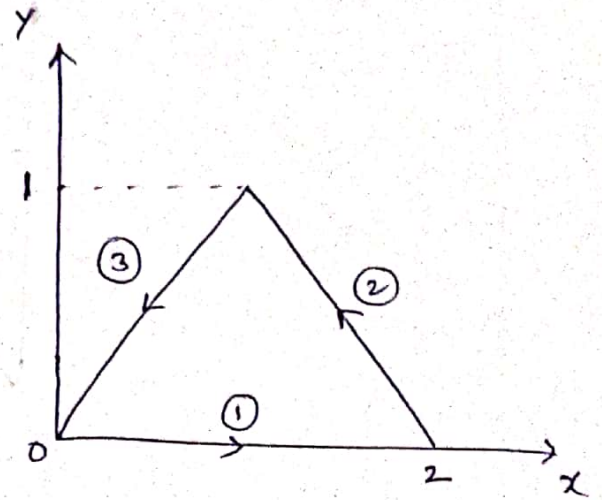
$$= \frac{4\mu_0 I}{4\pi(a/2)} \sqrt{2} \hat{k}$$

$$\boxed{\vec{B}_{\text{Total}} = \frac{\sqrt{2}}{a} \frac{\mu_0 I}{(a/2)} \hat{k}}$$

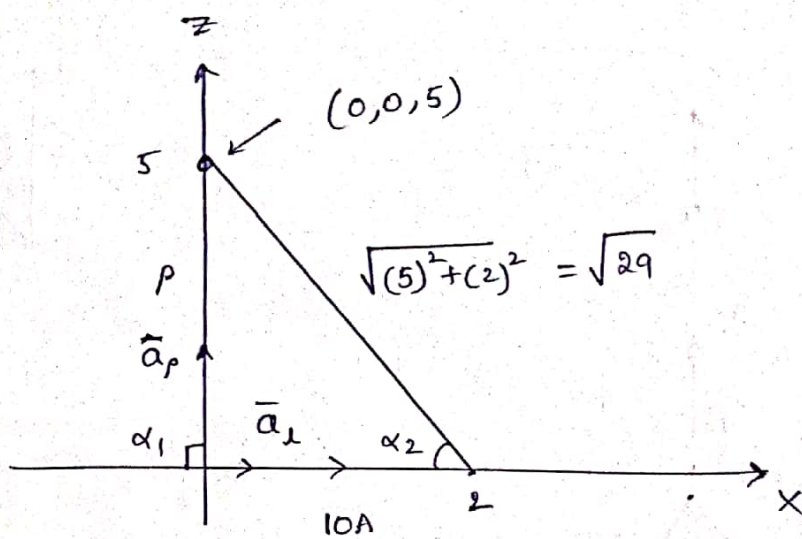
→ This is the field produced at the center of square loop.

=

- ⑦ The conducting triangular loop shown in figure carries a current  $10\text{A}$ . Find  $\vec{H}$  at  $(0,0,5)$  due to side 1 of the loop.



Sol:



From fig:  $\alpha_1 = 90^\circ$

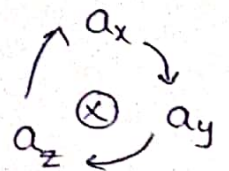
$$\cos \alpha_1 = \cos 90^\circ = 0$$

$$\alpha_2 = \frac{\pi}{2}$$

$$\cos \alpha_2 = \frac{2}{\sqrt{29}} ; p = 5$$

To find  $\vec{a}_\phi$  :  $\vec{a}_x \times \vec{a}_r = \vec{a}_\phi$

$$\vec{a}_x \times \vec{a}_z = -\vec{a}_y$$

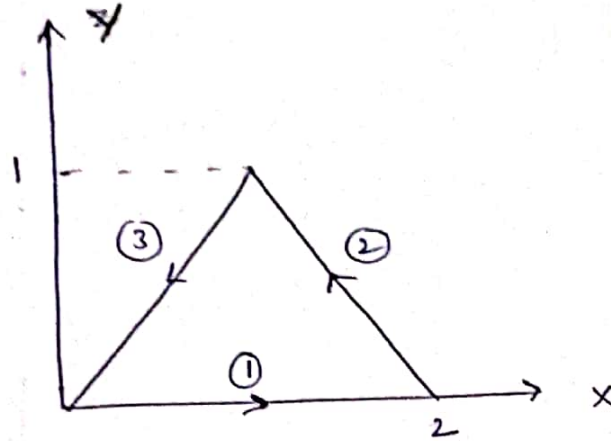


$$\text{Hence, } \vec{H} = \frac{I}{4\pi p} (\cos \alpha_2 - \cos \alpha_1) \vec{a}_\phi$$

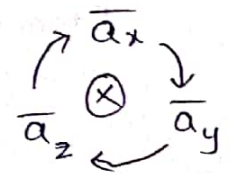
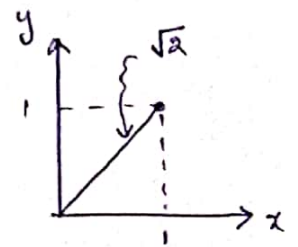
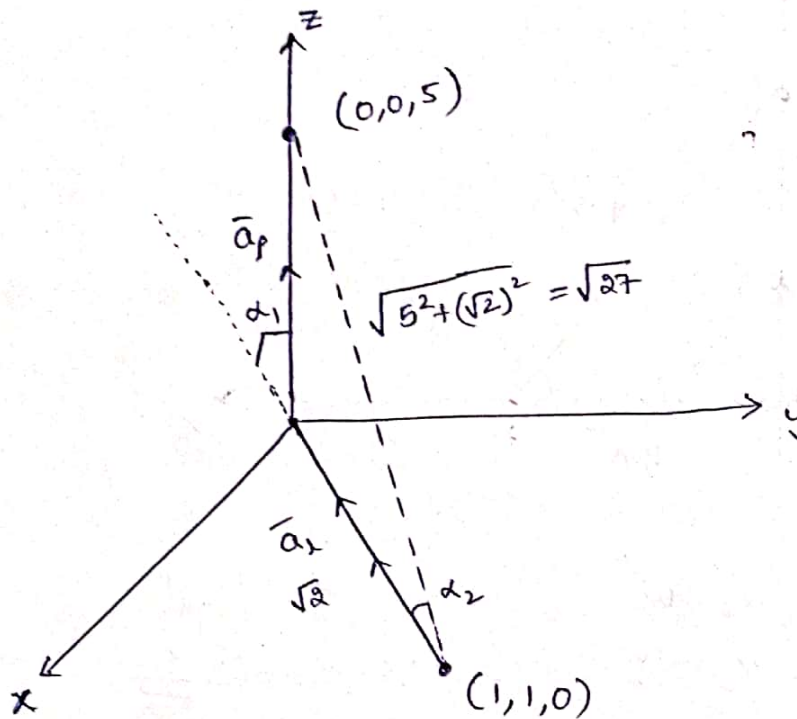
$$= \frac{10}{4\pi(5)} \left( \frac{2}{\sqrt{29}} - 0 \right) (-\vec{a}_y)$$

$$= 0.0591 (-\vec{a}_y) = -59.1 \vec{a}_y \text{ mA/m}$$

(P) Find  $\vec{H}$  at  $(0,0,5)$  due to Side 3 of the triangular loop carries current 10A shown in figure



Sol:



$$\cos \alpha_1 = \cos 90^\circ = 0$$

$$\cos \alpha_2 = \frac{\sqrt{2}}{\sqrt{27}} = \sqrt{\frac{2}{27}}$$

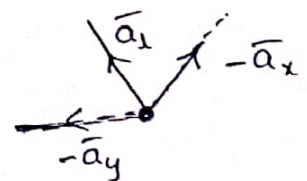
To determine:

$$\vec{a}_p = \vec{a}_x \times \vec{a}_y$$

$$= \left( \frac{-\vec{a}_x - \vec{a}_y}{\sqrt{2}} \right) \times \vec{a}_z$$

$$= \frac{-1}{\sqrt{2}} \{ \vec{a}_x \times \vec{a}_z + \vec{a}_y \times \vec{a}_z \}$$

$$= \frac{-1}{\sqrt{2}} [ -\vec{a}_y + \vec{a}_x ]$$



$$\vec{a}_1 = -\vec{a}_x - \vec{a}_y$$

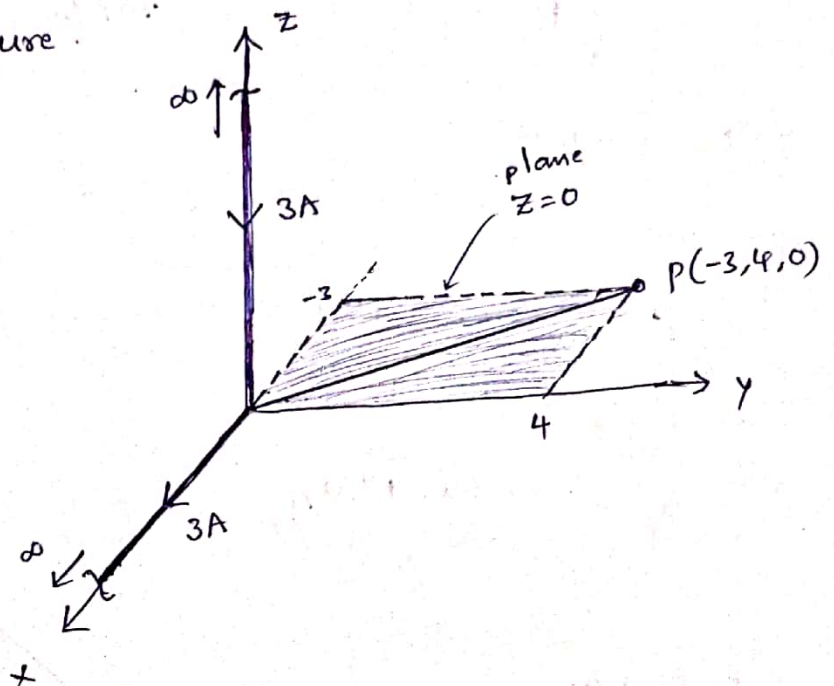
$$\vec{a}_1 = \frac{-\vec{a}_x - \vec{a}_y}{\sqrt{2}}$$

$$\vec{a}_p = \vec{a}_z$$

$$\begin{aligned}\therefore H_3 &= \frac{I}{4\pi r} (\cos \alpha_2 - \cos \alpha_1) \bar{a}_\phi \\ &= \frac{10}{4\pi(5)} \left( \frac{\sqrt{2}}{\sqrt{25}} - 0 \right) \left( \frac{-\bar{a}_x + \bar{a}_y}{\sqrt{2}} \right) \\ &= 0.03063 (-\bar{a}_x + \bar{a}_y)\end{aligned}$$

$$H_3 = -30.63 \bar{a}_x + 30.63 \bar{a}_y \text{ mA/m}$$

(P) Find  $\bar{H}$  at  $(-3, 4, 0)$  due to current filament shown in figure.



Sol:

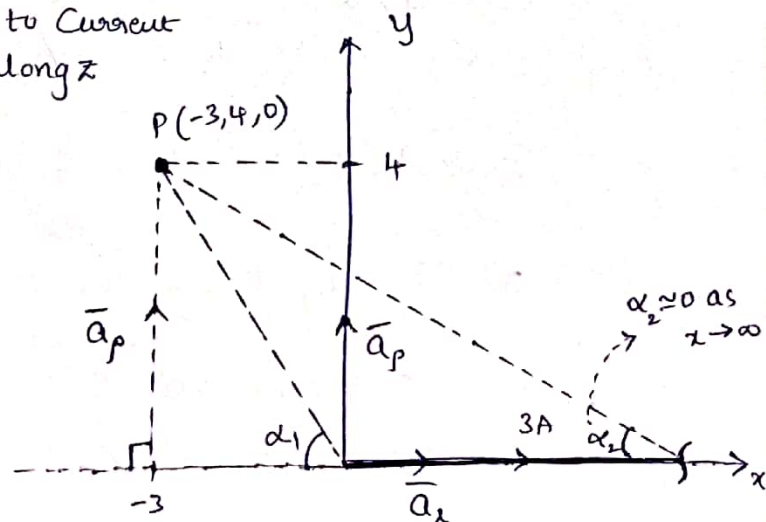
Let  $\bar{H} = \bar{H}_1 + \bar{H}_2 \dots$  at point  $P(-3, 4, 0)$

Due to current along x

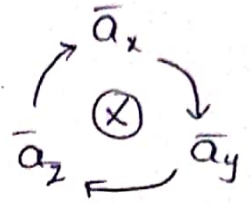
Due to current along z

$$\cos \alpha_1 = \frac{3}{\sqrt{4^2 + 3^2}} = \frac{3}{\sqrt{25}} = \frac{3}{5}$$

$$\cos \alpha_2 = \cos(0) = 1$$



To find,  $\bar{a}_\phi = \bar{a}_1 \times \bar{a}_\rho$   
 $= \bar{a}_x \times \bar{a}_y = \bar{a}_z$



To find  $\bar{H}_1$ :

$$\bar{H}_1 = \frac{I}{4\pi\rho} (\cos\alpha_2 - \cos\alpha_1) \bar{a}_\phi$$

$$= \frac{3}{4\pi(4)} \left(1 - \frac{3}{5}\right) \bar{a}_\phi$$

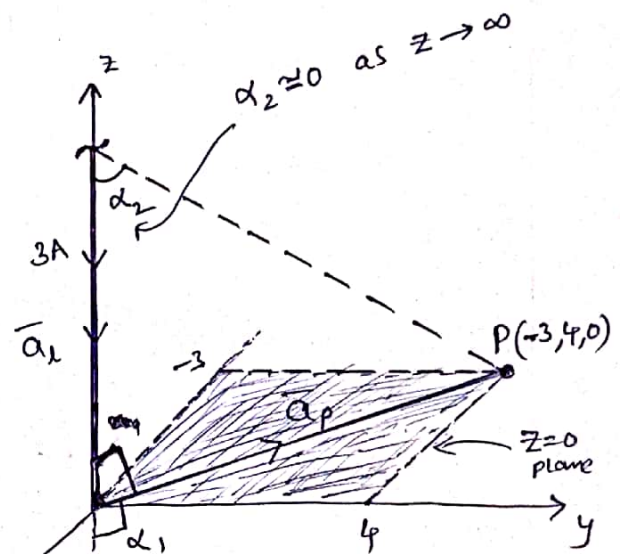
$$\boxed{\bar{H}_1 = 23.88 \bar{a}_z \text{ mA/m}}$$

To find  $\bar{H}_2$ :

$$\bar{\rho} = -3\bar{a}_x + 4\bar{a}_y$$

$$\rho = \sqrt{3^2 + 4^2} = \sqrt{25} = 5$$

$$\bar{a}_\rho = \frac{-3\bar{a}_x + 4\bar{a}_y}{5}$$



To find  $\bar{a}_\phi$

$$\bar{a}_\phi = \bar{a}_1 \times \bar{a}_\rho$$

$$= -\bar{a}_z \times \left( \frac{-3\bar{a}_x + 4\bar{a}_y}{5} \right)$$

$$= -\bar{a}_z \times \left( -\frac{3}{5} \bar{a}_x + \frac{4}{5} \bar{a}_y \right)$$

$$= \frac{3}{5} \bar{a}_y + \frac{4}{5} \bar{a}_x$$

$$\bar{a}_\phi = \left( \frac{4\bar{a}_x + 3\bar{a}_y}{5} \right)$$

$$\alpha_1 = 90^\circ$$

$$\alpha_2 = 0^\circ \text{ as } z \rightarrow \infty$$

$$\left\{ \begin{array}{l} \cos\alpha_1 = 0 \\ \cos\alpha_2 = 1 \end{array} \right\}$$

$$\vec{H}_a = \frac{I}{4\pi\rho} (\cos\alpha_2 - \cos\alpha_1) \vec{a}_\phi$$

$$= \frac{3}{4\pi(5)} (1-0) \cdot \vec{a}_\phi$$

$$= \frac{3}{4\pi(5)} \times \left( \frac{4\vec{a}_x + 3\vec{a}_y}{5} \right)$$

$$\vec{H}_a = 38.2 \vec{a}_x + 28.65 \vec{a}_y \text{ mA/m}$$

So  $\vec{H} = \vec{H}_1 + \vec{H}_a$

$$\vec{H} = 38.2 \vec{a}_x + 28.65 \vec{a}_y + 23.88 \vec{a}_z \text{ mA/m}$$

- (P) A circular loop located on  $x^2 + y^2 = a$ ,  $z = 0$  carries a <sup>direct</sup> current of 10A along  $\vec{a}_\phi$ . Determine  $\vec{H}$  at  $(0,0,4)$  and  $(0,0,-4)$ .

Sol:

At point  $(0,0,h)$

Using Biot-Savart's law

$$d\vec{H} = \frac{I d\vec{l} \times \vec{R}}{4\pi R^3}$$

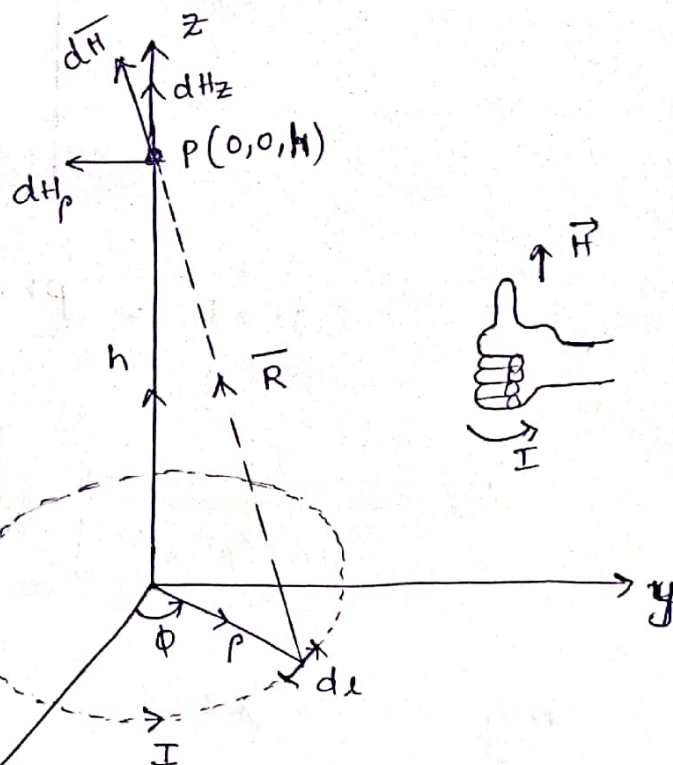
Cylindrical Co-ordinate System

$$d\vec{l} = d\rho \vec{a}_\rho + \rho d\phi \vec{a}_\phi + dz \vec{a}_z$$

Since  $\rho = \text{constant}$   
&  $z = 0$  for given loop

so,  $d\rho = dz = 0$

$$d\vec{l} = \rho d\phi \cdot \vec{a}_\phi$$



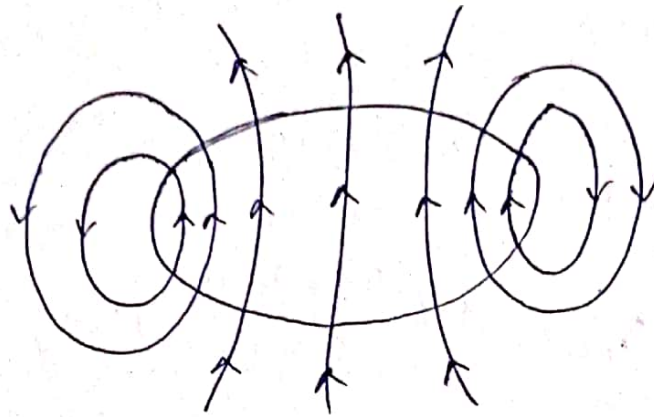


Fig: flux lines due to the current loop.

From Fig:

$$\rho \bar{a}_\rho + \bar{R} = h \bar{a}_z$$

$$\bar{R} = h \bar{a}_z - \rho \bar{a}_\rho$$

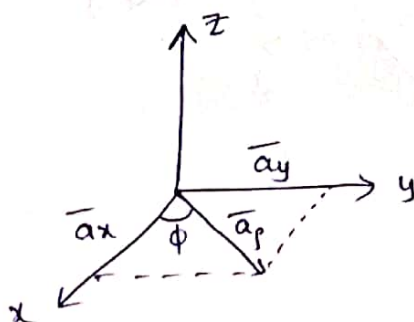
$$d\bar{l} \times \bar{R} = \begin{vmatrix} \bar{a}_\rho & \bar{a}_\phi & \bar{a}_z \\ 0 & \rho d\phi & 0 \\ -\rho & 0 & h \end{vmatrix}$$

$$d\bar{l} \times \bar{R} = \rho h d\phi \bar{a}_\rho + \rho^2 d\phi \bar{a}_z$$

$$d\bar{H} = \frac{I}{4\pi [(\rho^2 + h^2)^{3/2}]} \left\{ \cancel{\rho h d\phi \bar{a}_\rho} + \rho^2 d\phi \bar{a}_z \right\}$$

(by symmetry)

NOTE :



$$\bar{a}_\rho = \cos\phi \bar{a}_x + \sin\phi \bar{a}_y$$

Integrating  $\cos\phi$  &  $\sin\phi$  over  $0 \leq \phi < 2\pi$  gives Zero.

$$\vec{H} = \int d\vec{H} \vec{a}_z = \int \frac{I \rho^2 d\phi}{4\pi [\rho^2 + h^2]^{3/2}} \vec{a}_z$$

$$= \frac{I \rho^2 \vec{a}_z}{4\pi [\rho^2 + h^2]^{3/2}} \int_0^{2\pi} d\phi$$

$$= \frac{I \rho^2 \vec{a}_z}{2 \cdot 4\pi [\rho^2 + h^2]^{3/2}} \cdot 2\pi$$

$$\boxed{\vec{H} = \frac{I \rho^2 \vec{a}_z}{2 [\rho^2 + h^2]^{3/2}}}$$

---> MFI at point  $(0,0,h)$   
due to circular current  
loop (at  $z=0$ ) having  
radius  $\rho$ .

To find  $\rho$ :  $x^2 + y^2 = \rho^2$   
 $x^2 + y^2 = (3)^2 \dots \dots$  given  
 so,  $\rho = 3$ .

(a) At  $(0,0,4)$

put  $I = 10A$ ,  $h = 4$

$$\vec{H}(0,0,4) = \frac{10(3)^2}{2 [9 + 16]^{3/2}} \vec{a}_z$$

$$= 0.36 \vec{a}_z \text{ A/m}$$

(b) At  $(0,0,-4)$ ,  $h = -4$ ,  $I = 10A$

$$\vec{H} = \frac{I \rho^2}{2 (\rho^2 + h^2)^{3/2}} \vec{a}_z = \frac{10(3)^2 \vec{a}_z}{2 [9 + (-4)^2]^{3/2}} = 0.36 \vec{a}_z \text{ A/m}$$

So  $\vec{H}(0,0,4) = \vec{H}(0,0,-4) = 0.36 \vec{a}_z \text{ A/m}$

(P)

planes  $z=0$  and  $z=4$  carry current  $K = -10\hat{a}_x$  A/m and  $K = 10\hat{a}_x$  A/m, respectively. Determine  $\vec{H}$  at

- (a)  $(1, 1, 1)$  (b)  $(0, -3, 10)$

Sol:

The parallel ~~sheets~~ current sheets are shown in Figure

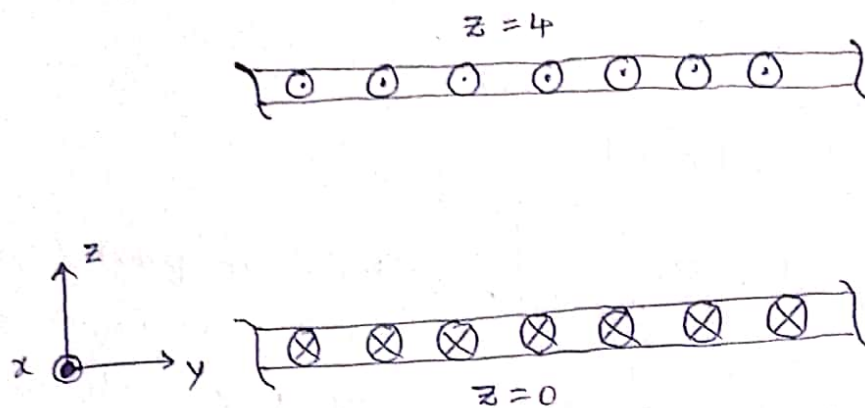


Fig: parallel infinite current sheets

$$\text{Let } \vec{H} = \vec{H}_0 + \vec{H}_4$$

where  $H_0$  and  $H_4$  are the contributions due to current sheets  $z=0$  and  $z=4$  respectively.

- (a) At  $(1, 1, 1)$ , which is between the plates ( $0 < z=1 < 4$ )

$$H_0 = \frac{1}{2} K \times \hat{a}_n = \frac{1}{2} (-10\hat{a}_x) \times \hat{a}_z = 5\hat{a}_y \text{ A/m}$$

$$H_4 = \frac{1}{2} K \times \hat{a}_n = \frac{1}{2} (10\hat{a}_x) \times (-\hat{a}_z) = 5\hat{a}_y \text{ A/m}$$

$$\text{Hence } \vec{H} = 10\hat{a}_y \text{ A/m}$$

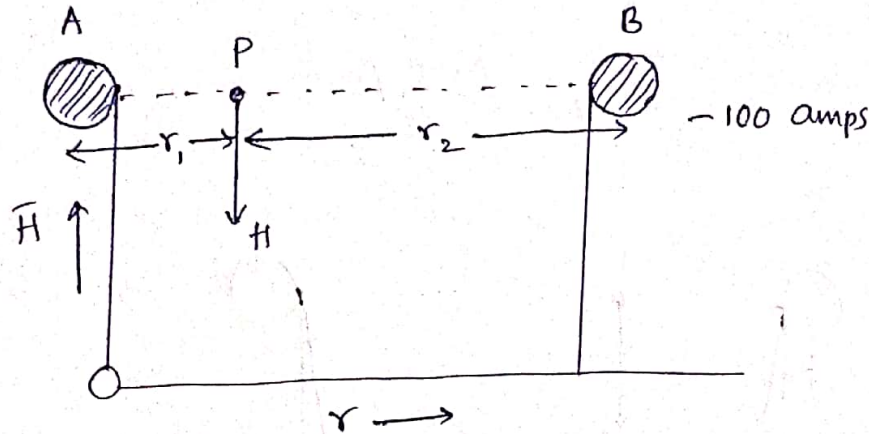
- (b) At  $(0, -3, 10)$ , which is above the two sheets ( $z=10 > 4 > 0$ )

$$H_0 = \frac{1}{2} K \times \hat{a}_n = \frac{1}{2} (-10\hat{a}_x) \times \hat{a}_z = 5\hat{a}_y \text{ A/m}$$

$$H_4 = \frac{1}{2} K \times \hat{a}_n = \frac{1}{2} (10\hat{a}_x) \times \hat{a}_z = -5\hat{a}_y \text{ A/m}$$

$$\text{Hence } \vec{H} = 0 \text{ A/m.}$$

- ⑦ A single phase circuit comprises two parallel conductors A & B, 1 cm diameter and spaced 1 m apart. The conductors carry currents of +100 and -100 amps, respectively. Determine the field intensity at the surface of each conductor and also in the space exactly midway between A & B.



Sol

Field at any point 'p' between A & B is

$$\begin{aligned} H &= H_A + H_B \\ &= \frac{I}{2\pi r_1} + \frac{I}{2\pi r_2} \\ &= \frac{I}{2\pi} \left[ \frac{1}{r_1} + \frac{1}{r_2} \right] \end{aligned}$$

H at conductor surface

$$\begin{aligned} \bar{H} &\cong \frac{100}{2\pi} \left[ \frac{1}{1 \times 10^{-2} \times \frac{1}{2}} + \frac{1}{1} \right] \\ &= \frac{100}{2\pi} \left[ \frac{100}{0.5} + \frac{1}{1} \right] \\ &= \frac{10050}{\pi} \text{ Amp/m} \end{aligned}$$

$\bar{H}$  at midway between A & B

$$= \frac{I}{2\pi(0.5)} + \frac{I}{2\pi(0.5)}$$

$$= \frac{100}{\pi} \times 4$$

$$= \frac{200}{\pi} \text{ Amps/m.}$$

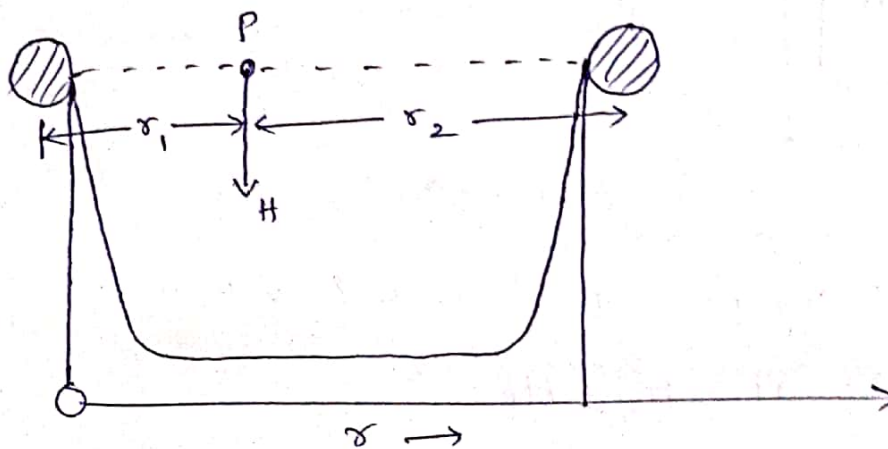


Fig: Variation of  $\bar{H}$  b/w A & B.